### A computational continuum model of poroelastic beds

(Limitations and possibilities)

Uğis Lācis<sup>1</sup>, Shervin Bagheri<sup>1</sup> and Sudhakar Yogaraj<sup>1</sup>

<sup>1</sup>Linné FLOW Centre, KTH Mechanics







Inspiration from nature

















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Inspiration from nature







All of these animals move in the surrounding medium (fluid) and interact with it.











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Inspiration from nature

#### There are different surface textures<sup>1</sup> used by motile animals

<sup>1</sup>Liu, K. & Lei, J., Bio-inspired design of multiscale structures for function integration, *Nano Today* **6(2)**, 155-175 (2011).





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Main aim of this work





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Main aim of this work



Understand how the porous and elastic multi-scale surface texture interact with freely moving fluid





#### Outline

- Motivation and objective
- Illustration and methods
- Governing equations
- Response to flow vortex
- Limitations and applicability
- Conclusions and outlook





#### Outline

#### Motivation and objective

#### Illustration and methods

Poroelastic bed Multi-scale expansion

Governing equations

Response to flow vortex

Limitations and applicability

Conclusions and outlook





Poroelastic bed





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Poroelastic bed







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Poroelastic bed





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Poroelastic bed



• System is inherently multi-scale,  $\epsilon = l/H \lesssim 0.1$ 





Method overview

Direct numerical simulations are often not feasible due to extreme computational requirements





Method overview

Direct numerical simulations are often not feasible due to extreme computational requirements





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Method overview

Direct numerical simulations are often not feasible due to extreme computational requirements



How to do this mathematically without free parameters?





Scale separation and estimates

Scale estimates are important for physical understanding of problem and to later apply mathematical framework





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Scale separation and estimates

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Scale separation and estimates

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Scale separation and estimates



 $U^d \sim \frac{l^2 \Delta P}{\mu H}$ 





Scale separation and estimates



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Scale separation and estimates



$$U^d \sim \frac{l^2 \Delta P}{\mu H}; \quad U^d \sim \left(\frac{l}{H}\right)^2 U^f$$





Scale separation and estimates



$$U^d \sim \frac{l^2 \Delta P}{\mu H}; \quad U^d \sim \left(\frac{l}{H}\right)^2 U^f; \text{ shear} \sim \frac{U^f}{H};$$





Multi-scale expansion

• Scale separation parameter  $\epsilon = l/H \lesssim 0.1$ 





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- Slow (micro) coordinate  $x_1 = x$
- Fast (macro) coordinate  $x_0 = \epsilon x$





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- Expansion in both coordinate and amplitude

  - ▶ Derivative  $()_{,i} = ()_{,i_1} + \epsilon ()_{,i_0}$ ▶ Variable  $f = f^{(0)} + \epsilon f^{(1)} + \epsilon^2 f^{(2)} + ...$







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Group terms at different orders, solve, homogenize, ...





#### Outline

Motivation and objective

Illustration and methods

Governing equations Poroelastic bed Interface conditions

Response to flow vortex

Limitations and applicability

Conclusions and outlook





#### **Governing equations**

Poroelastic bed





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#### **Governing equations**

Poroelastic bed

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► Free fluid, Navier-Stokes:

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = -\nabla p + \frac{1}{Re} \nabla^2 \vec{u}$$
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#### **Governing equations**

Poroelastic bed

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Poroelastic material, linear elasticity:

$$\rho \frac{\partial^2 \vec{v}}{\partial t^2} = \nabla \cdot \left[ \mathbf{C} \quad : \frac{1}{2} \left\{ \boldsymbol{\nabla} \vec{v} + \left( \boldsymbol{\nabla} \vec{v} \right)^T \right\} \right]$$





0


Poroelastic bed

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#### Poroelastic material, linear elasticity:

$$(1-\theta)\rho\frac{\partial^2 \vec{v}}{\partial t^2} = \nabla \cdot \left[\mathbf{C}^{\text{ef}}: \frac{1}{2}\left\{\boldsymbol{\nabla} \vec{v} + (\boldsymbol{\nabla} \vec{v})^T\right\}\right]$$



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Poroelastic bed

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#### Additional information in book<sup>2</sup>

 $<sup>^2\</sup>mbox{Mei},$  C. C. & Vernescu, B., Homogenization methods for multiscale mechanics, *World scientific* (2010)





Interface conditions





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Interface conditions





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Interface conditions



Interface treatment is non-trivial



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Interface conditions, velocity





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Interface conditions, velocity



#### Additional information in publication<sup>3</sup>

<sup>3</sup>Lācis, U. & Bagheri, S., A framework for computing effective boundary conditions at the interface between free fluid and a porous medium, *J. Fluid Mech.* **812**, 866-889 (2017)





Interface conditions, velocity

• Decomposing fast flow:  $\vec{u} = \vec{U} + \vec{u}^+$ ,  $p = P + p^+$ 



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Perturbations driven mostly by shear stress:

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 $\pmb{\Sigma}^U\cdot \hat{n}$ 

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$$\pmb{\Sigma}^U \cdot \hat{n} + \pmb{\Sigma}^{u^+} \cdot \hat{n} = \pmb{\Sigma}^{u^-} \cdot \hat{n}$$

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Interface conditions, velocity

$$\vec{u} = -\frac{\mathbf{K}}{\mu} \cdot \boldsymbol{\nabla} p^{-} + \mathbf{L} : \left[ \boldsymbol{\nabla} \vec{u} + (\boldsymbol{\nabla} \vec{u})^{T} \right]$$

Generalized BJ<sup>4</sup> condition without any empirical parameters<sup>3</sup>

<sup>&</sup>lt;sup>3</sup>Lācis, U. & Bagheri, S., A framework for computing effective boundary conditions at the interface between free fluid and a porous medium, *J. Fluid Mech.* **812**, 866-889 (2017)



<sup>&</sup>lt;sup>4</sup>Beavers, G. S. & Joseph, D. D., Boundary conditions at a naturally permeable wall, *J. Fluid Mech.* **30(01)**, 197-207 (1967)



Interface conditions, velocity



Generalized BJ condition without any empirical parameters<sup>3</sup>

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Interface conditions, velocity



$$\vec{u} = \frac{\partial_t \vec{v}}{\partial_t \vec{v}} - \frac{\mathbf{K}}{\mu} \cdot \nabla p^- + \mathbf{L} : \left[ \nabla \vec{u} + (\nabla \vec{u})^T \right]$$

Generalized BJ condition without any empirical parameters<sup>3</sup>

▶ Permeability  $\mathbf{K} \sim l^2$  and slip length  $\mathbf{L} \sim l$ , disappears as  $l \rightarrow 0$ 

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Interface conditions, stress





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A continuum model of poroelastic beds - 14 of 20



Interface conditions, stress



Natural way to match free fluid and poroelastic material







Interface conditions, stress



- Natural way to match free fluid and poroelastic material
- We propose to use the total stress continuity

$$\left[\mathbf{C}^{\text{ef}}:\frac{1}{2}\left(\boldsymbol{\nabla}\vec{v}+\left(\boldsymbol{\nabla}\vec{v}\right)^{T}\right)-\boldsymbol{\alpha}p^{-}\right]\cdot\hat{n}=\left[-p\boldsymbol{\delta}+\frac{1}{\boldsymbol{Re}}\left(\boldsymbol{\nabla}\vec{u}+\left(\boldsymbol{\nabla}\vec{u}\right)^{T}\right)\right]\cdot\hat{n}$$





### Outline

Motivation and objective

Illustration and methods

Governing equations

Response to flow vortex Flow field Displacement field

Limitations and applicability

Conclusions and outlook





Flow field<sup>5</sup>







Flow field<sup>5</sup>







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Flow field<sup>5</sup>







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Flow field<sup>5</sup>







Displacement field<sup>5</sup>








#### Displacement field<sup>5</sup>







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### Outline

Motivation and objective

Illustration and methods

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Response to flow vortex

Limitations and applicability What we cannot capture What we can describe

Conclusions and outlook





What we cannot capture



Illustration through breakdown of riblet drag reduction<sup>6</sup>





What we cannot capture



Illustration through breakdown of riblet drag reduction<sup>6</sup>





What we cannot capture





FIGURE 15. General structure of a drag reduction curve.

Illustration through breakdown of riblet drag reduction<sup>6</sup>





What we cannot capture



Illustration through breakdown of riblet drag reduction<sup>6</sup>





What we cannot capture



Illustration through breakdown of riblet drag reduction<sup>6</sup>





What we cannot capture



- Illustration through breakdown of riblet drag reduction<sup>6</sup>
- Current model is limited to L = const

$$\vec{u} = \mathbf{L} : \left[ \nabla \vec{u} + \left( \nabla \vec{u} \right)^T \right]$$





What we cannot capture



- Illustration through breakdown of riblet drag reduction<sup>6</sup>
- Current model is limited to  $\mathbf{L} = const$ , could have  $\mathbf{L} = f(shear, ...)$

$$\vec{u} = \mathbf{L} : \left[ \nabla \vec{u} + \left( \nabla \vec{u} \right)^T \right]$$



What we cannot capture



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$$\vec{u} = \mathbf{L} : \left[ \nabla \vec{u} + \left( \nabla \vec{u} \right)^T \right] + \dots$$



What we can describe



FIGURE 15. General structure of a drag reduction curve.

Riblet drag reduction linear part<sup>7</sup>





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FIGURE 15. General structure of a drag reduction curve.

- Riblet drag reduction linear part<sup>7</sup>
- Current model can add (anisotropic) porosity

<sup>&</sup>lt;sup>7</sup>Luchini, P., Manzo, F., & Pozzi, A., Resistance of a grooved surface to parallel flow and cross-flow, *J. Fluid Mech.* **228**, 87-109 (1991)







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FIGURE 15. General structure of a drag reduction curve.

'Viscous regime'

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 $\frac{\Delta \tau}{\tau_0}$ 

-10%

0



20



FIGURE 15. General structure of a drag reduction curve.

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- Riblet drag reduction linear part<sup>7</sup>
- Current model can add (anisotropic) porosity, (anisotropic) elasticity

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0

-10%







FIGURE 15. General structure of a drag reduction curve.

- Riblet drag reduction linear part<sup>7</sup>
- Current model can add (anisotropic) porosity, (anisotropic) elasticity
- Examples in nature mostly anisotropic





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Conclusions

Model of flow above poro-elastic material with no empirical parameters





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### Model of flow above poro-elastic material with no empirical parameters

- Model equations and boundary conditions have been developed
- Model simulation has been validated with fully resolved simulation
- Poroelastic material response to free flow vortex has been explained





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### Limitations and applicability

- Model can not capture micro-scale variations
- Model is valid for linear regime in drag reduction curve





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- Model can not capture micro-scale variations
- Model is valid for linear regime in drag reduction curve

### All model codes (FreeFEM++) available in Github





Outlook

### Applying the developed model

- Adding porosity to riblets<sup>8</sup>
- Testing anisotropic poroelastic models
- Most examples from nature anisotropic





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### Applying the developed model

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### Extending the model

Complement the model with two-phase flow



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### Extending the model

- Complement the model with two-phase flow
- Investigate response to shear, pressure, ...

	water	
L	air	

<sup>8</sup>Yogaraj, S., ongoing work with NEK5000



A continuum model of poroelastic beds – 20 of 20



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A continuum model of poroelastic beds – 20 of 20



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# **Conclusions and outlook**

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- Testing anisotropic poroelastic models
- Most examples from nature anisotropic

### Extending the model

- Complement the model with two-phase flow
- Investigate response to shear, pressure, ...
- Understand stability from system energy



<sup>8</sup>Yogaraj, S., ongoing work with NEK5000



# Thank you for your attention!

### Questions and discussion





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Displacement field<sup>8</sup>







Displacement field<sup>8</sup>







Displacement field<sup>8</sup>







Displacement field<sup>8</sup>







Displacement field<sup>8</sup>





<sup>8</sup>Lācis, U., Zampogna, G. A. & Bagheri, S., A computational continuum model of poroelastic beds, *Proc. R. Soc. A.* **473**, 20160932 (2017)





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