Thermal fluctuations of an interface near a contact line

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Introduction

- The understanding and modelling of the dynamics of wetting and contact lines, such as spreading or motion of a droplet on a solid surface, is a subject at the forefront of physics, chemistry, and engineering;
- The **regularization** at the contact line is an essential ingredient: within all the descriptions provided in the literature, the physics near the contact line is **oversimplified** since **thermal fluctuations are ignored**;
- Our goal is to **start a different line of thought** to investigate **fluctuating contact lines** at the microscopic scale:
 - 1) How thermal fluctuations behave close to a contact line?
 - 2) Thermal fluctuations alone can provide any form of microscopic regularization within a purely local fluctuating hydrodynamic framework?
- The first step is then to consider a **static contact line** on a homogeneous substrate in presence of **thermal fluctuations**.



Mathematical framework



Profile probability
$$P_{R}[h] \propto e^{-\theta_{\rm Y}^2 \frac{R}{2\ell}} e^{-\frac{1}{2\ell} \int_{0}^{R} dx \, h'(x)^2}$$

Thermal lenght
$$\ell = k_{\rm B}T/\gamma$$

$$\ell \, (\partial \ln c / \partial h)_{h=0} = -\theta$$

Mathematical framework



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- Study the statistics of the contact point, i.e. P(R);
- Study the average profiles, i.e. (h(x));
- Quantify the thermal regularization, i.e. a.

Two dimensionless parameters

- $S = \theta_Y h_0 / \ell$ (scale separation): tells us how much thermal fluctuations can distort the interface;
- $\tau = \theta/\theta_{\rm Y}$ (intensity of interactions): it parametrizes the microscopic binding effects close to the solid substrate.

Thermal lenght

$$\ell = k_{\rm B} T / \gamma$$

Impenetrability
 $\ell (\partial \ln c / \partial h)_{h=0} = -\theta$

Contact point probability

$$P(R) = \frac{1-\tau}{2} \left[\sqrt{\frac{2S}{\pi R}} e^{S(1-\frac{R}{2}-\frac{1}{2R})} + \tau S e^{S(1-\tau)[1-(1+\tau)\frac{R}{2}]} \operatorname{erfc}\left(\frac{1-\tau R}{\sqrt{2R/S}}\right) \right]$$



Average profile and binding potential

Average profile

$$\langle h(x) \rangle = \frac{\tau}{(1+\tau)^2} \frac{e^{S(1-\tau)[1-(1+\tau)\frac{x}{2}]}}{\sqrt{S}} \operatorname{erfc}\left(\frac{1-\tau x}{\sqrt{2x/S}}\right) - \frac{x-1}{2/\sqrt{S}} \operatorname{erfc}\left(\frac{x-1}{\sqrt{2x/S}}\right) \\ - \left[\frac{\tau}{(1+\tau)^2} \frac{1}{\sqrt{S}} + \frac{1-\tau}{1+\tau} \frac{x+1}{2/\sqrt{S}}\right] e^{2S} \operatorname{erfc}\left(\frac{x+1}{\sqrt{2x/S}}\right) + \frac{2}{1+\tau} \sqrt{\frac{x}{2\pi}} e^{-\frac{(x-1)^2}{2x/S}}$$



Conclusions

- We have investigated the effect of thermal fluctuations on the morphology of an interface near a contact line in the presence of an impenetrable wall;
- We have introduced the right ensemble (integration over *R*) where Young's angle is robust, and the inner physics depends on a boundary condition parameter θ that represents the microscopic deviation from Young's angle;
- The impenetrable nature of the boundary leads to a "repulsion" of capillary waves from the wall and the interactions between the fluctuating interface and the wall are captured in terms of an effective binding potential of finite range, solely induced by thermal fluctuations;
- Pseudo-partial wetting states emerge similarly to a phase transition in the model $(\langle R \rangle \rightarrow \infty)$, depending on the micromechanics parameter θ ;
- **Open issue**: Derivation of θ from inner model. Then, and then only, we may expect to predict the conditions under which a pseudo-partial wetting transition can be observed in a real three-dimensional case.

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Thanks for your attention!