



Technische Universität München



Yielding of amorphous materials

Alessio Zaccone

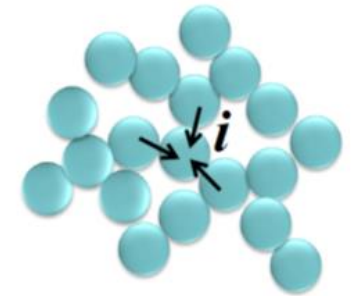
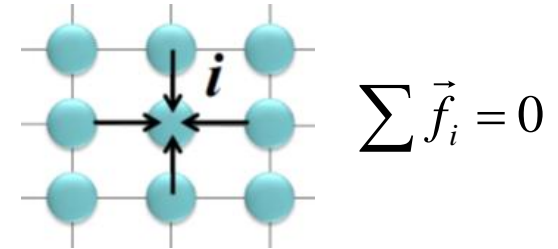
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TU Munich

Non-affine deformations

The breaking of local inversion symmetry is the cause for non-affinity. This is a key in disordered solids.

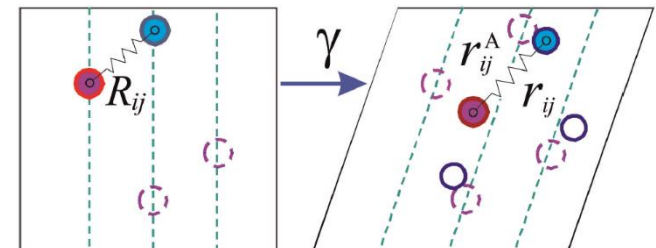
Q: But there are many non-centrosymmetric crystals: what about them?

→ In fact, it is known since Kelvin (1890) that crystals with no inversion symmetry (piezoelectrics, e.g. quartz) all have a very low shear modulus!



The associated addition to the elastic free energy is always negative (relaxation of local forces) and can be presented as:

$$F = F_A - F_{NA} = F_A - \frac{1}{2} \left(\frac{\partial \vec{f}_i}{\partial \gamma} \cdot \frac{\partial \vec{r}_{i,NA}}{\partial \gamma} \right) \gamma^2$$



Non-affine deformations

The non-affine reduction of shear modulus can be calculated for harmonic central forces (with spring constant κ):

$$F = F_A - F_{NA} = F_A - \frac{1}{2} \left(\frac{\partial \vec{f}_i}{\partial \gamma} \cdot \frac{\partial \vec{r}_{NA}}{\partial \gamma} \right) \gamma^2$$

Born (1940) in affine model

Non-affine softening for harmonic central forces gives a factor $z_c = 2d$

$$G \approx \frac{N}{V} \kappa r_0^2 (z - z_c)$$

Maths can be found in:


Zaccone & Scossa-Romano PRB (2011)

Zaccone, Blundell, Terentjev PRB (2011)

Q: How limiting is this? What if there are constraints: non-central forces or excluded volume?

→ In a few cases (bond-bending & excl. volume) analytical solutions are possible.

What does the temperature do?

We now know: $G \approx \frac{N}{V} \kappa r_0^2 (z - z_c)$  $G \approx \left(\frac{\kappa}{r_0} \right) \phi \cdot (z - z_c)$

Relate $(z - z_c)$ to the density

The probability $g(r)$ of having two soft particles separated by a vector of length r displays a divergence

$$g(r) \sim (r - r_0)^{-1/2}$$

O'Hern, Silbert, Liu, Nagel, 2003

The increment $\delta z = (z - z_c) \sim \int g(r) r^2 dr$

which now gives $(z - z_c) \sim \sqrt{\phi - \phi_c}$

This gives the temperature change of the shear modulus


Relate density to temperature

Thermal expansion cf. of a solid

$$\alpha_T = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)$$

Replace V by f , and integrate:

$$\ln \phi = -\alpha_T \cdot T + \text{const}$$



$$(z - z_c) = \sqrt{\phi_c [e^{\alpha_T (T_c - T)} - 1]}$$

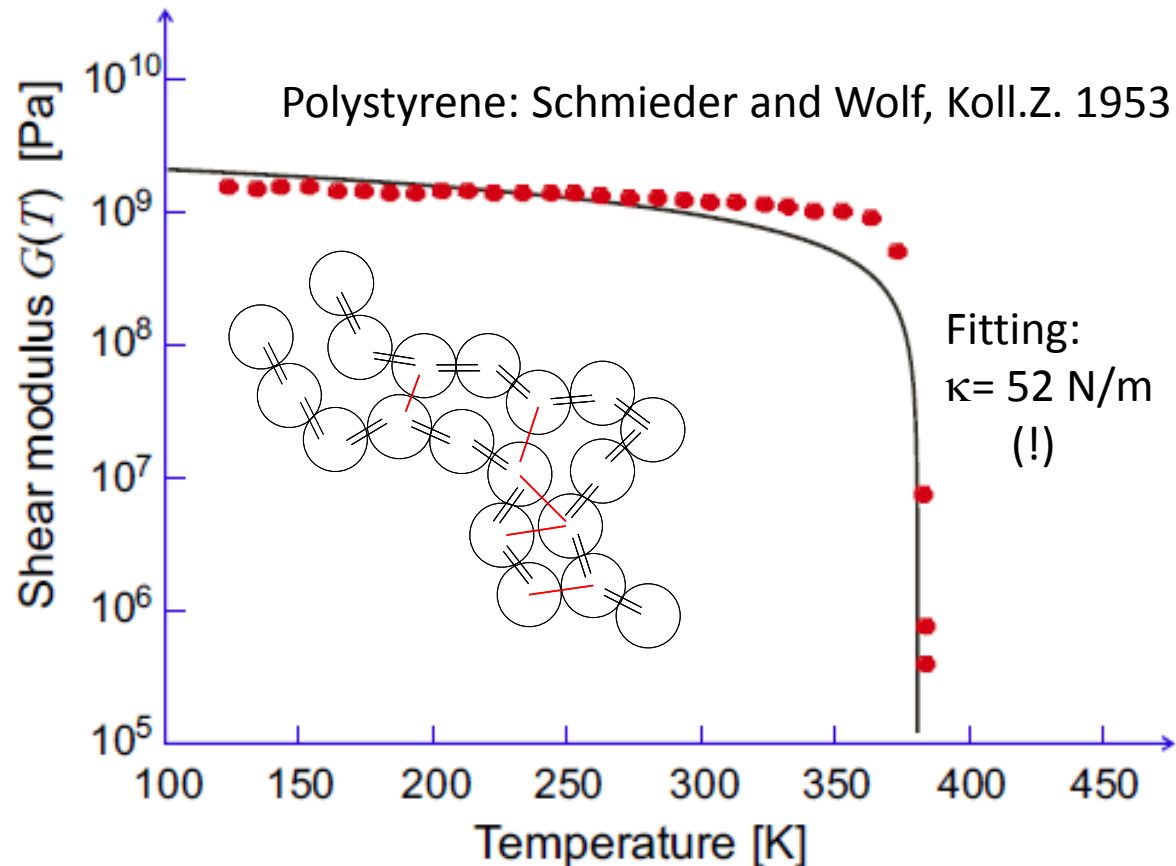
Comparing with glassy polymer ($T < T_g$)

We found: $G \approx \frac{N}{V} \kappa r_0^2 (z - z_c)$ \longrightarrow $G \approx \frac{\kappa}{r_0} \varphi_c e^{\alpha_T (T_c - T)} \sqrt{\varphi_c [e^{\alpha_T (T_c - T)} - 1]}$

The system must be free to expand. In that case, a recent MD simulation for LJ glass has confirmed

$$(z - z_c) \sim \sqrt{\phi - \phi_c}$$

Wittmer et al., JCP 2013



Zaccone & Terentjev PRL (2013)

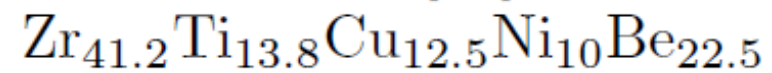
Plan for today:

Two examples of fluidization:

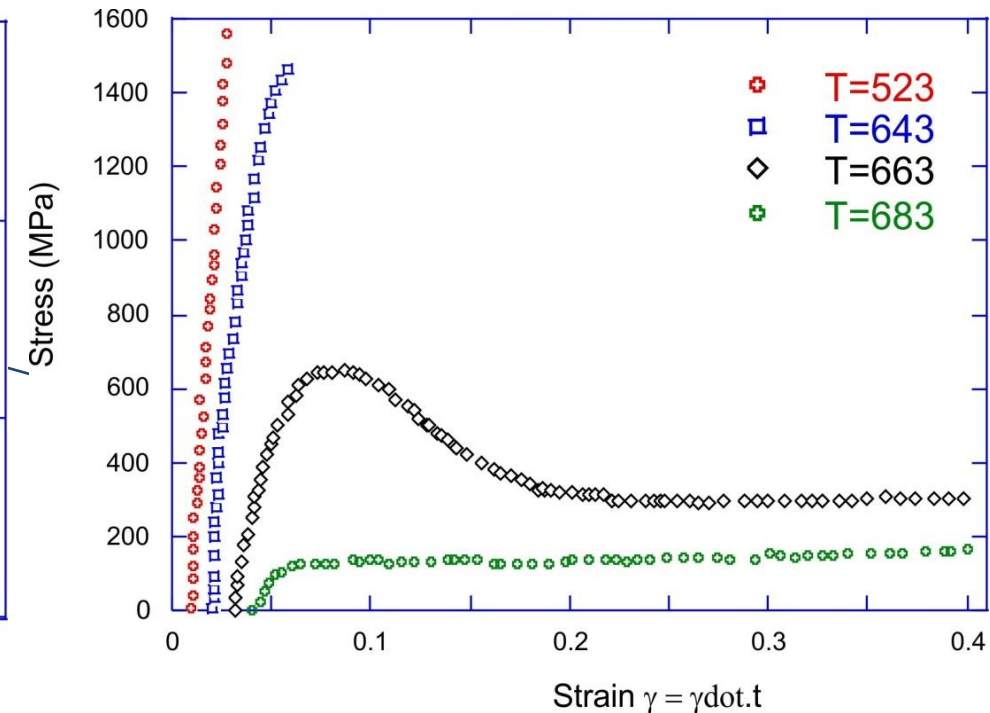
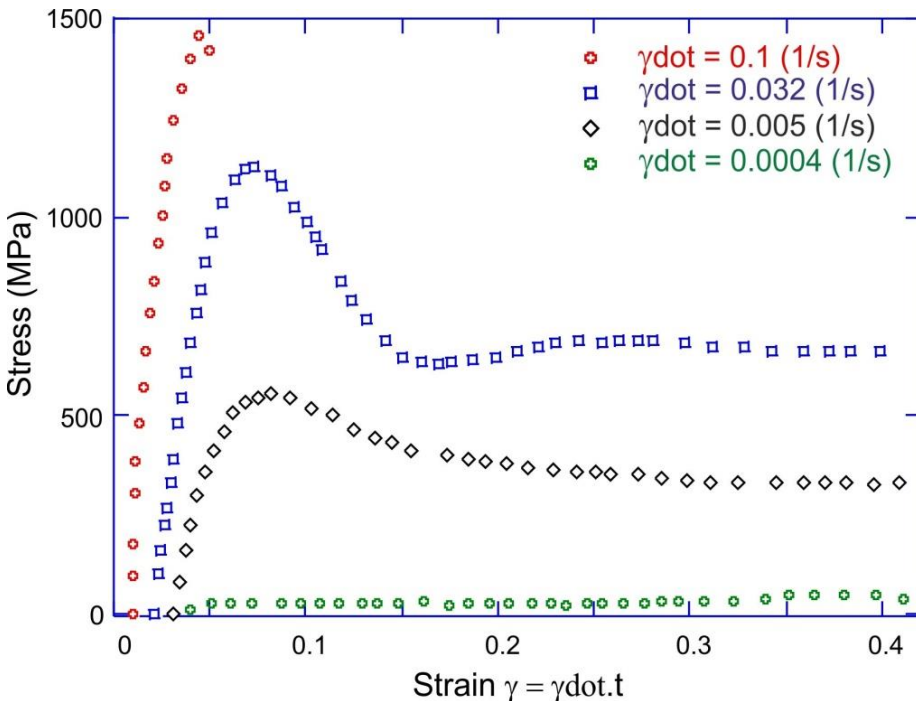
1. How a rigid disordered solid (glass) approaches a melting point ($G \rightarrow 0$) on increasing **temperature**. This is essentially a “glass transition” examined from below T_g
2. How a rigid disordered solid (glass) yields and starts plastic flow at **finite deformation rate**. Why is there a ‘stress overshoot’?

Can we fluidize the random solid by shear?

Experiment on metallic glass

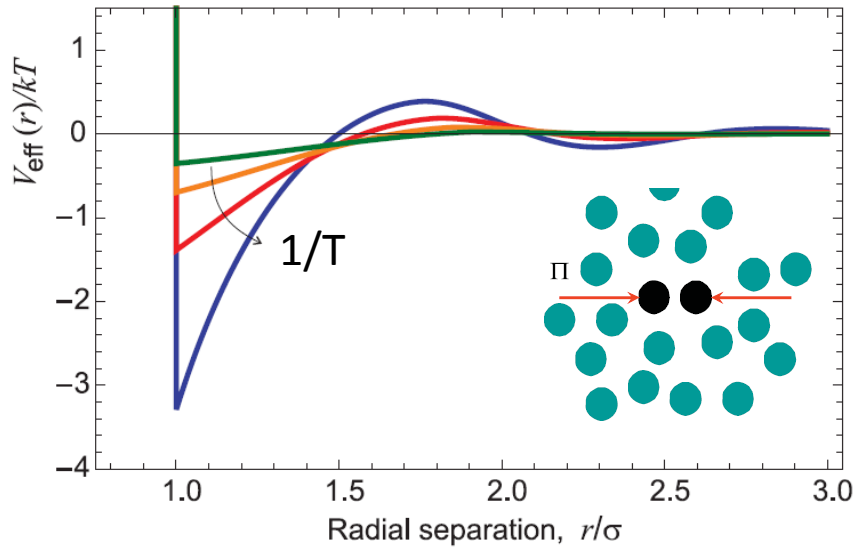


Lu, Ravichandran, Johnson, ActaMater. 2003



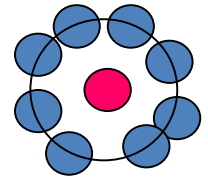
The linear modulus
The overshoot
The plastic flow stress

Shear-induced cage deformation



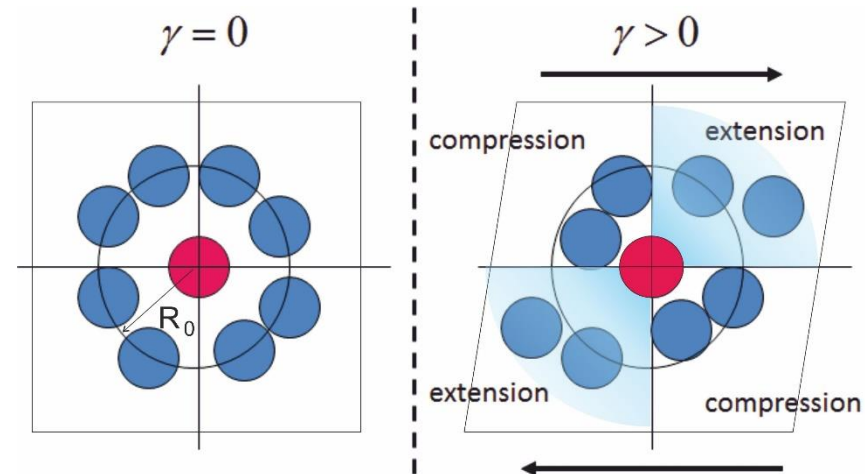
$$g(r) = \exp[-V_{\text{eff}} / kT]$$

Potential of mean force, accounts also for the “cage”

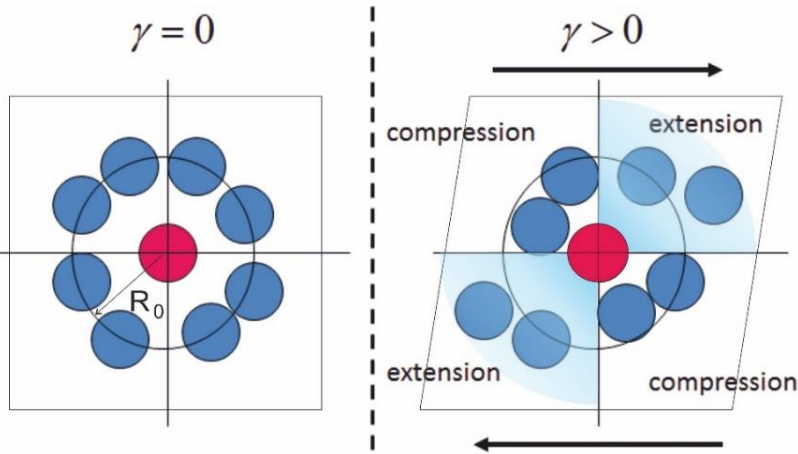


$$g(\mathbf{r}, \gamma) = \exp[-V_{\text{eff}} / kT + h(\mathbf{r})\gamma]$$

Particles escaping from the cage under shear (extensional sector) go to fill free volume spots (dilatancy is negligible)

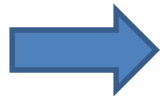
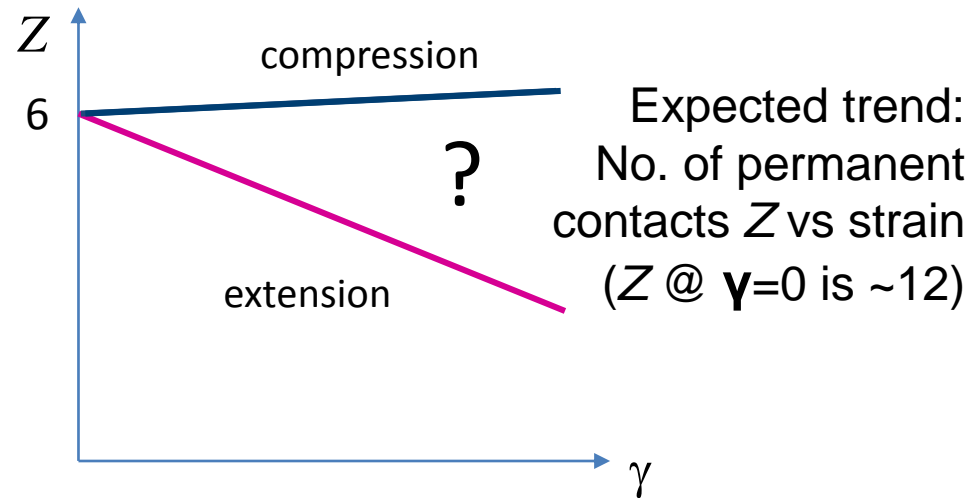


Av. number of contacts z decreases with $\gamma \uparrow$



Only bonds which are **'permanent'**, within the bonding minimum, contribute to elasticity: fluctuating 'fluid' contacts should be discarded

Net decrease of 'permanent' contacts: imbalance between extension sector (particles "peeled off") and compression sector ("crowding")



Evolution of permanent Z can be measured in confocal microscopy of colloidal glasses or in simulations (in progress)

Stress non-linearity for a strain ramp (start-up shear)

We saw it many times: $G \approx \frac{N}{V} \kappa r_0^2 (z - z_c) \rightarrow F_{el} = \frac{1}{2} K [z(\gamma) - z_c] \cdot \gamma^2$

z is calculated from $g(r)$

$$z = \int g(r) 4\pi r^2 dr$$

$g(r)$ relaxes towards equilibrium

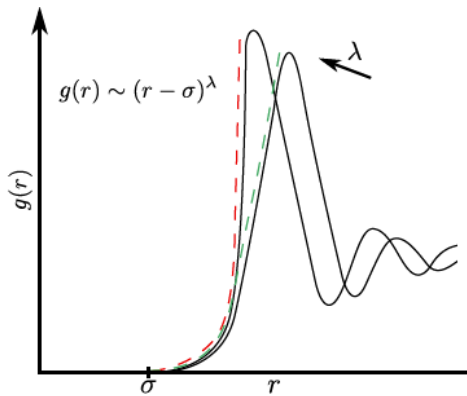
$$g(r) = \Psi_1(r) \cdot e^{-t/\tau_1}$$

lowest eigenvalue

“time is γ ”

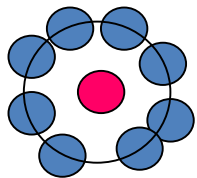
$$t = \gamma / \dot{\gamma}$$

at constant rate



We obtain the contact number z as a function of shear strain γ

$$z(\gamma) = z_0 \cdot \frac{1}{2} (1 + e^{-t/\tau_s}) = \frac{1}{2} z_0 (1 + e^{-A\gamma})$$



The exponent: $A = \frac{1}{\dot{\gamma} \tau_s} + \frac{\Delta}{k_B T}$

half of the sectors deplete at $\gamma \gg 1$

The values: $z_{MAX} = z_0 \approx 12, z_c = 6$

(only central forces)

Stress non-linearity during a strain ramp (start-up shear)

We substitute $z(\gamma)$: $F_{el} = \frac{1}{2} K [z(\gamma) - z_c] \cdot \gamma^2$ and differentiate for $\sigma(\gamma)$:

➡ Elastic stress: $\sigma_{el}(\gamma) = \frac{1}{4} z_0 K e^{-A\gamma} \cdot \gamma(2 - A\gamma) + \frac{1}{2} (z_0 - 2z_c) K \cdot \gamma$

Please remember: $A = \frac{1}{\dot{\gamma} \tau_s} + \frac{T_g}{T}$

That's good, but we must not forget the stress relaxation (viscoelastic effect).

This produces the second part: $\sigma_{visc}(\gamma) = \int G(s) \cdot \dot{\gamma} ds$

Within the simplest (Zener) model: $G(t) = G + G_R e^{-t/\tau_v}$ and $\tau_v = \eta / G_R$

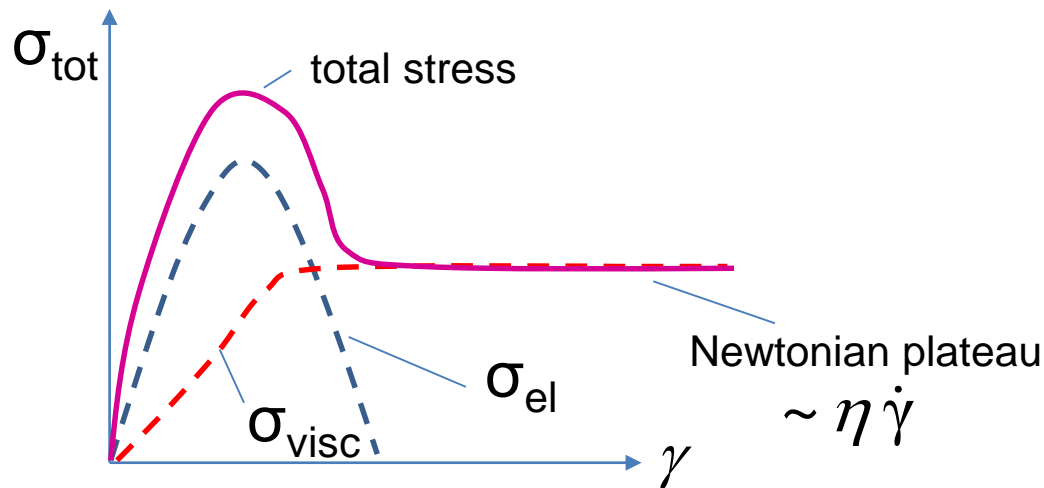
➡ Finally: $\sigma_{tot} = \sigma_{el}(\gamma) + \eta \dot{\gamma} \left(1 - e^{-\gamma / \dot{\gamma} \tau_v} \right)$

Stress rise, overshoot and the plastic flow

Apply a constant shear ramp $\gamma = \dot{\gamma} \cdot t$

and the glassy solid responds with the stress:

$$\sigma_{\text{tot}} \approx \frac{1}{4} z_0 K e^{-\gamma \left(\frac{T_g}{T} + \frac{1}{\dot{\gamma} \tau_s} \right)} \gamma (2 - A\gamma) + \eta \dot{\gamma} \left(1 - e^{-\frac{\gamma}{\dot{\gamma} \tau_v}} \right)$$



YIELD POINT ($G=0$)

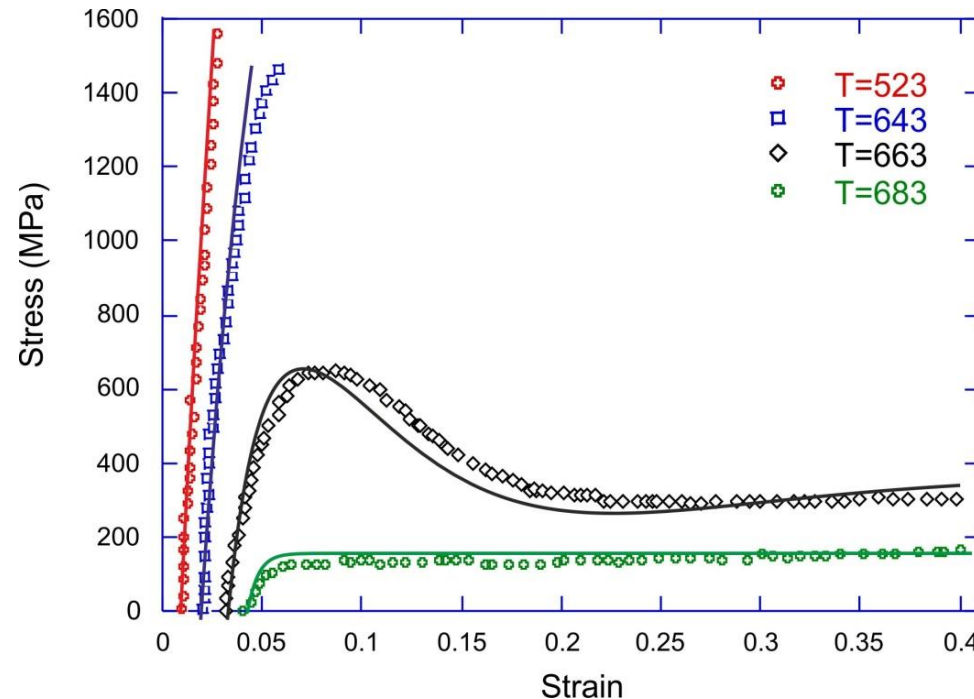
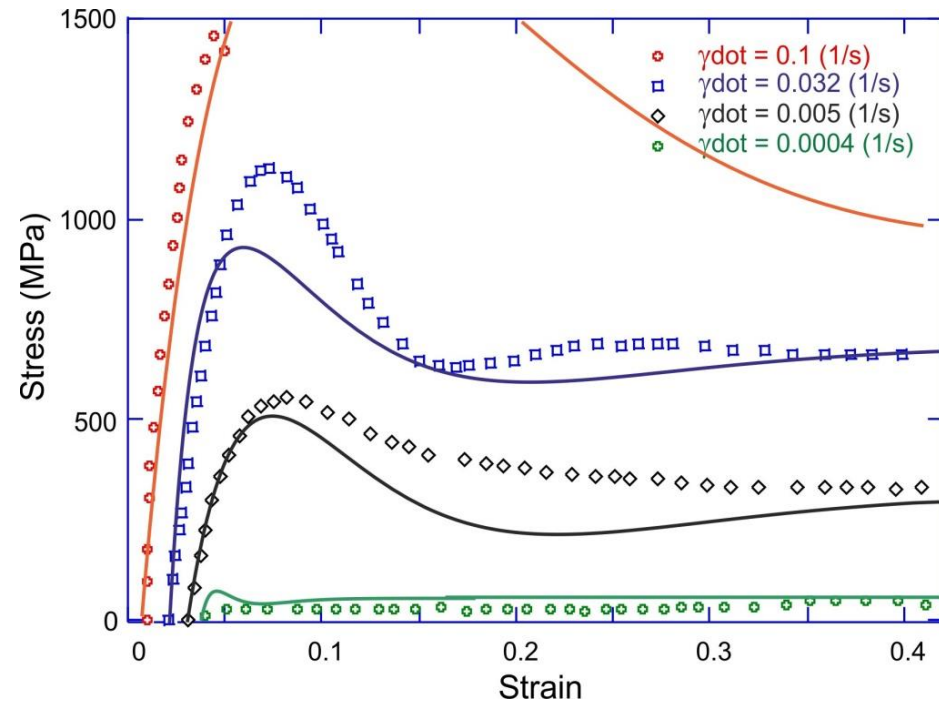
$$\gamma_{\text{CR}} \approx \frac{1}{2A} = \frac{0.5}{T_g / T + 1 / \dot{\gamma} \tau_s}$$

Stress rise, overshoot and the plastic flow

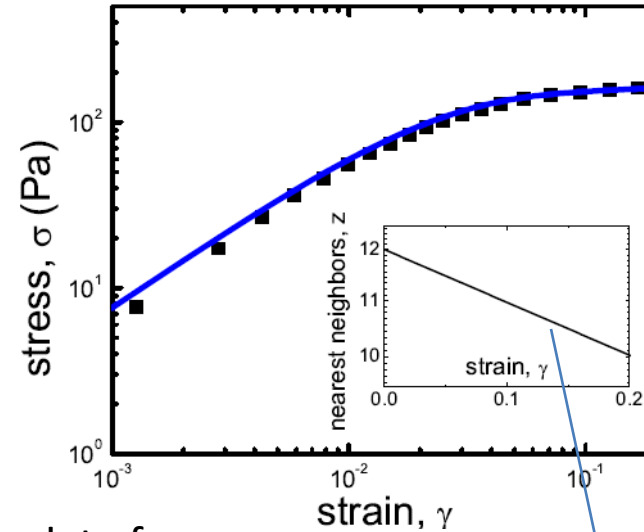
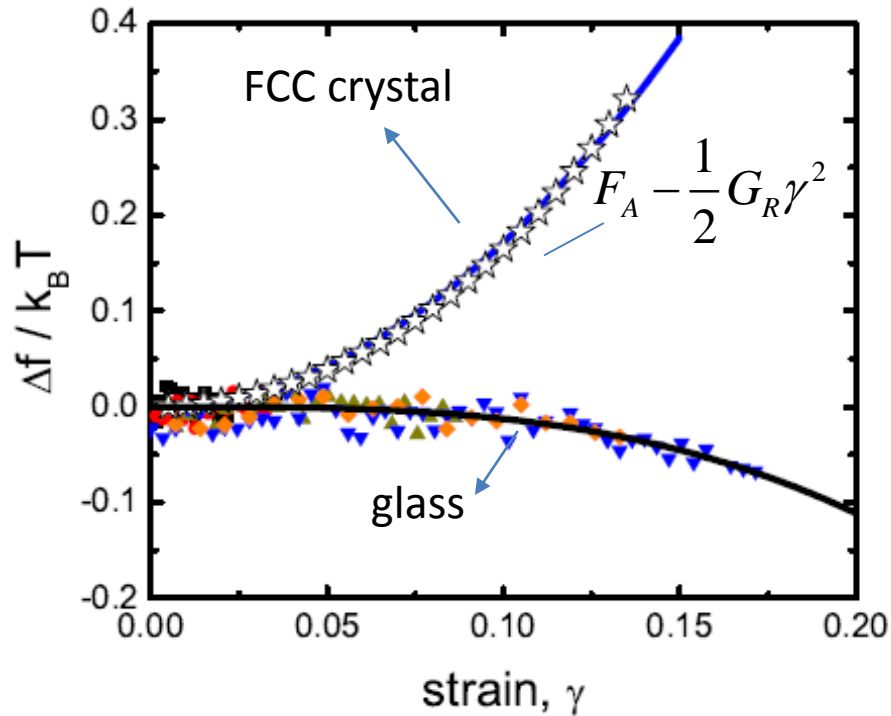
Shear ramp: $\gamma = \dot{\gamma} \cdot t$

$$\text{Stress: } \sigma_{\text{tot}} \approx \frac{1}{4} z_0 K e^{-\gamma \left(\frac{T_g}{T} + \frac{1}{\dot{\gamma} \tau_s} \right)} \gamma (2 - A\gamma) + \eta \dot{\gamma} \left(1 - e^{-\frac{\gamma}{\dot{\gamma} \tau_v}} \right)$$

Only two t-parameters are not measured experimentally by Johnson et al.



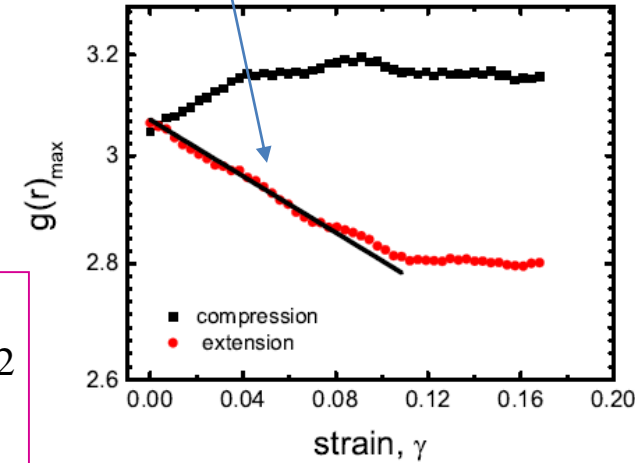
Yielding of colloidal glasses: comparing with experiments



data from
P. Schall's group

free energy of deformation of colloidal glasses

$$F = F_A - F_{NA} = F_A - \frac{1}{2} \left(\frac{\partial \vec{f}_i}{\partial \gamma} \cdot \frac{\partial \vec{r}_{NA}}{\partial \gamma} \right) \gamma^2 - \frac{1}{2} G_R \gamma^2$$



Conclusion

We used the simplified model of central harmonic bonds and the linear theory of non-affine elastic deformations produces a useful form of the shear modulus, $G \sim K[z - z_c]$

Examining how the average number of contacts z changes in different circumstances allows practical problems to be solved

1. Using **thermal expansion** ideas, and connecting $z-f(T)$ via $g(r)$, we produced a model of **glass melting**, as well as the T_g
2. Using the **compression-extension** sectors asymmetry in shear, we found $z(\gamma)$ and were able to describe the **yielding** of metallic glass and the of colloidal glass in agreement with several experimental data-sets

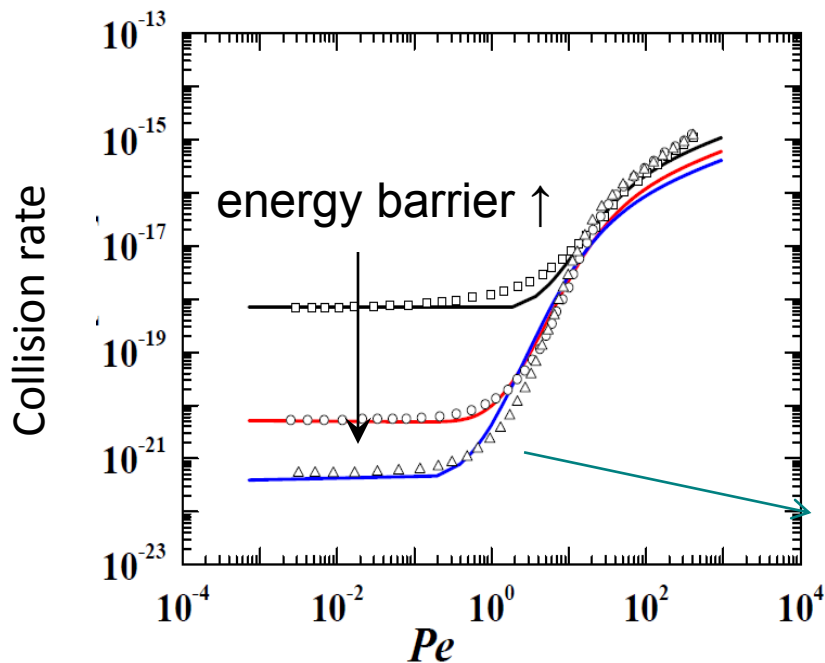
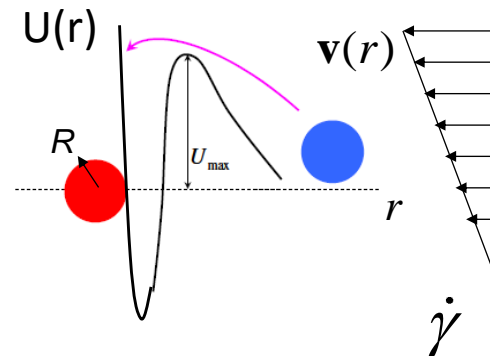
Diffusion-advection: analytical solution

$$\frac{\partial \rho}{\partial t} = \nabla \cdot (D \nabla \rho + b \rho \nabla U - b \nabla \rho)$$

diffusion

intermolecular interactions

linear flow field



analytical solution:
Zaccone, et al. PRE (2009),
PRL (2011)

ballistic limit

$$rate \propto \dot{\gamma} (2R)^3$$

recovered at $Pe = \infty$

$$rate \propto e^{-\beta U_{\max} + 2\alpha Pe}$$

$$Pe = \frac{6\pi\mu\dot{\gamma}R^3}{kT}$$

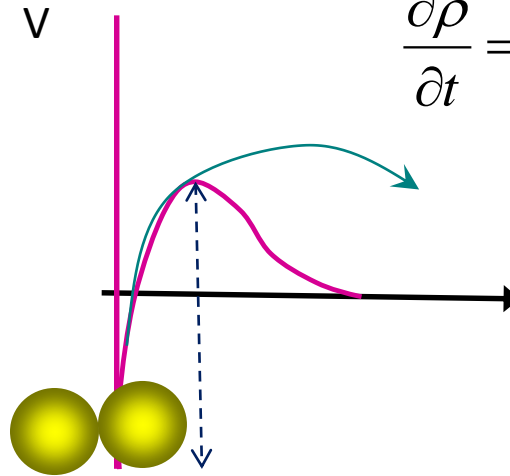
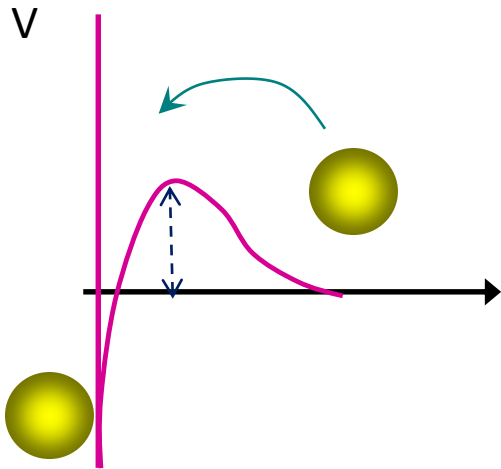
ANALYTICAL SOLUTION: collision rate

$$K_{1,1} = \frac{8\pi D_0 R c_0}{2 \int_0^{\delta/R} \frac{dx}{\mathcal{G}(x)(x+2)^2} \exp \int_{\delta/R}^x dx \left(\beta \frac{dU}{dx} + Pe \tilde{v}_r \right)}$$

Can we predict the cluster breakup rate?

self-assembly

breakup



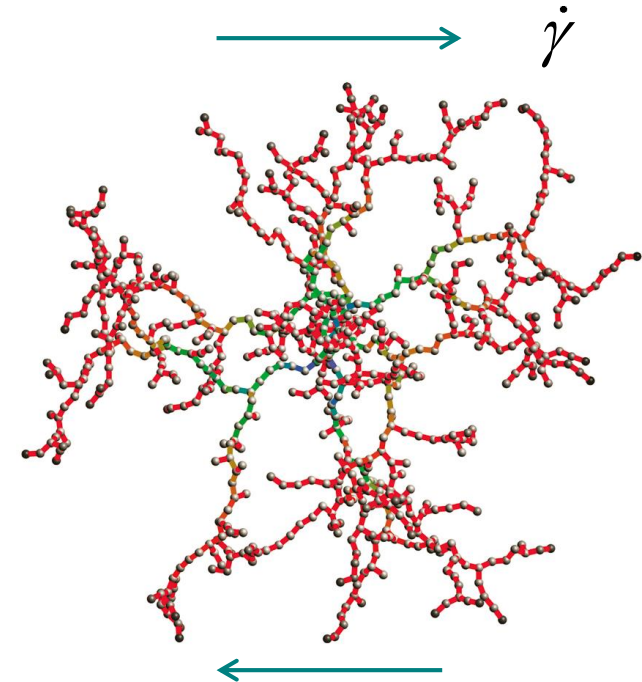
$$\frac{\partial \rho}{\partial t} = \nabla \cdot (D \nabla \rho + b \rho \nabla V - b \nabla \rho)$$

collective stress-transmission through the aggregate

$$\begin{aligned} \tilde{V}_{\text{eff}} &= V_{\text{eff}} - \Gamma b (N/2) \int \langle v_r \rangle dr \\ &= V - b(1 + \Gamma N/2) \int \langle v_r \rangle dr - 2k_B T \ln(r/a) \end{aligned} \propto \dot{\gamma}$$

$$\Gamma = (R_g/a)^\alpha,$$

$$\alpha = -2.06491d_f - 0.0180344/(3 - d_f) + 4.98585$$

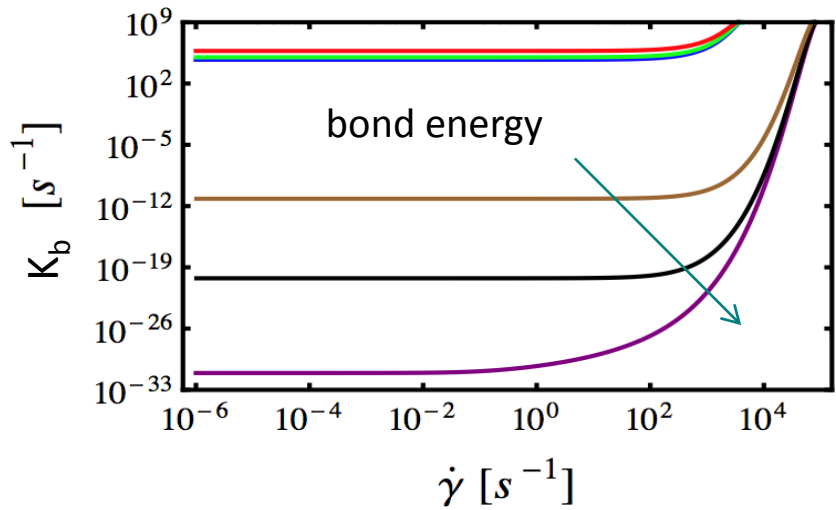


first physical theory
of aggregate breakup rate

Conchuir & Zaccone, PRE 2013

$$K_{ij}^- = \frac{\sqrt{-\tilde{V}_{\text{eff}}''(r_{\text{max}})\tilde{V}_{\text{eff}}''(r_{\text{min}})}}{2\pi b \exp[\beta\tilde{V}_{\text{eff}}(r_{\text{max}}) - \beta\tilde{V}_{\text{eff}}(r_{\text{min}})]}$$

Successful description of several experimental data



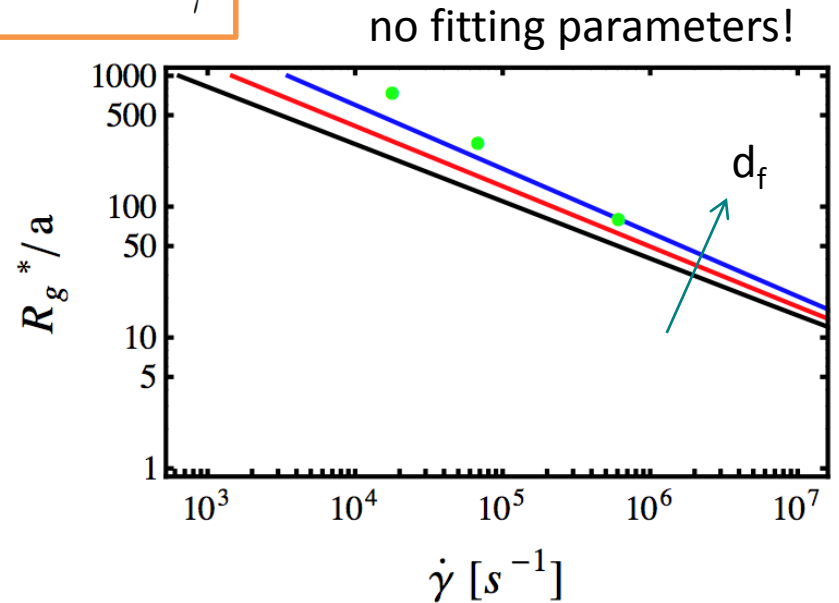
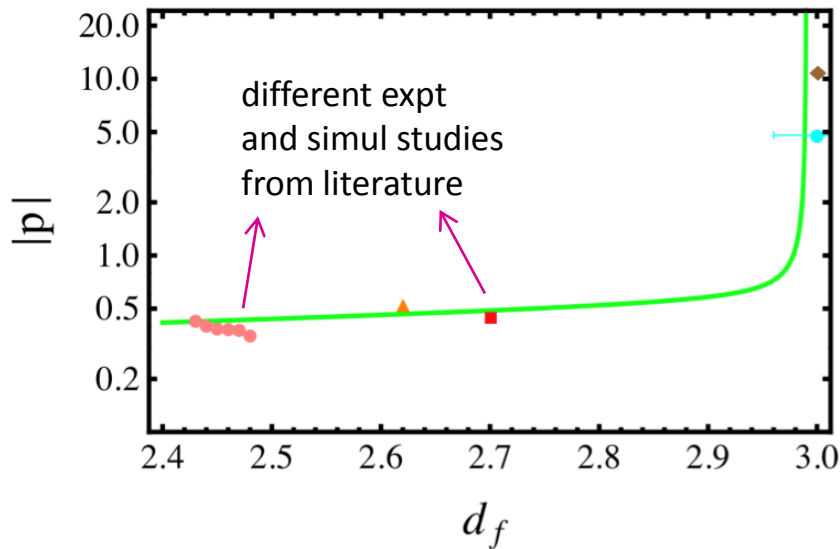
$$K_b = \frac{\sqrt{-\tilde{V}_{\text{eff}}''(r_{\text{max}})\tilde{V}_{\text{eff}}''(r_{\text{min}})}}{2\pi b \exp[\underbrace{\beta\tilde{V}_{\text{eff}}(r_{\text{max}}) - \beta\tilde{V}_{\text{eff}}(r_{\text{min}})}_{=0}]}$$

=0
instantaneous breakup
(no activation energy)

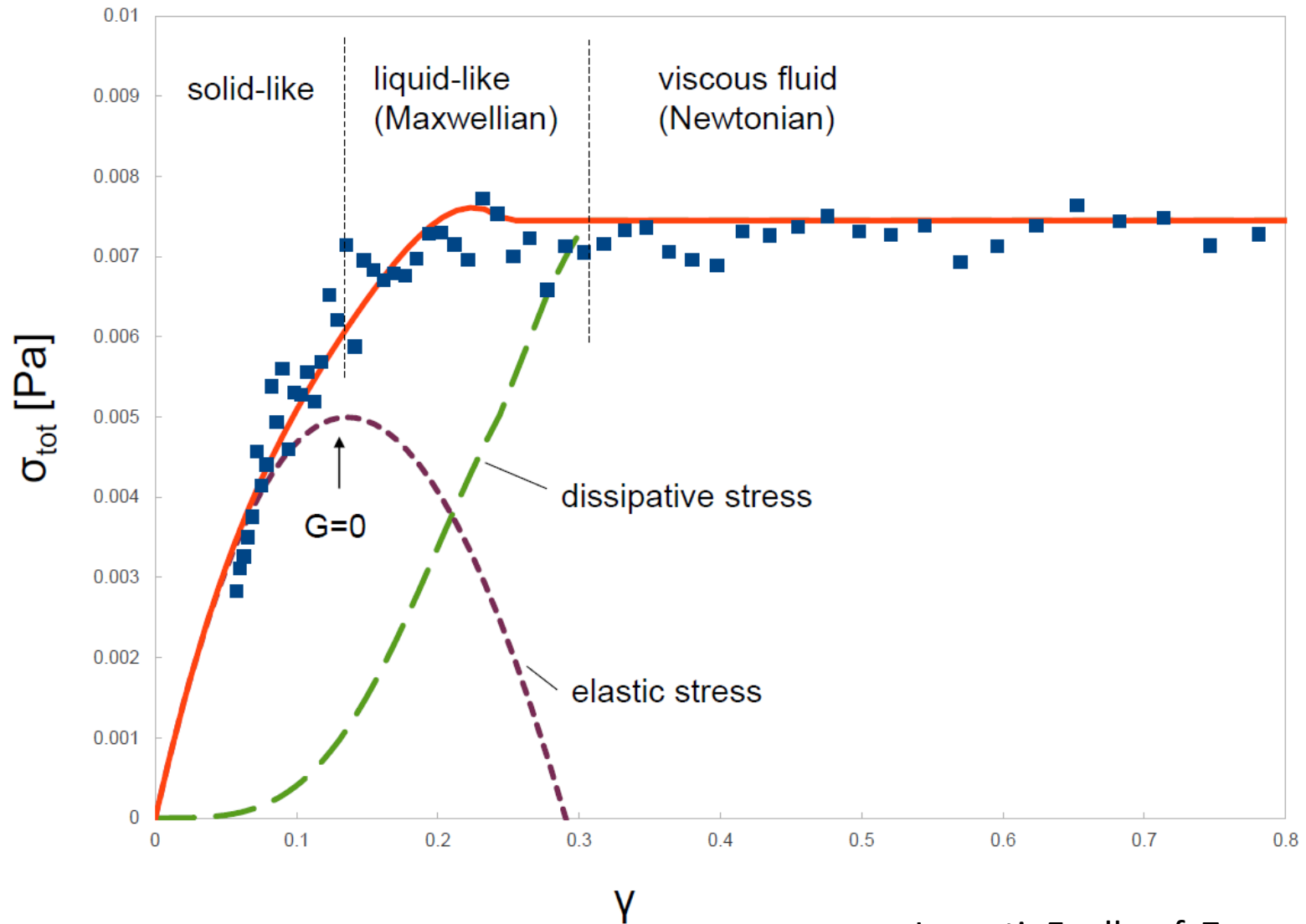


$$R_g^* \sim \dot{\gamma}^{-\frac{1}{d_f + \alpha(d_f)}} \sim \dot{\gamma}^p$$

max cluster size surviving



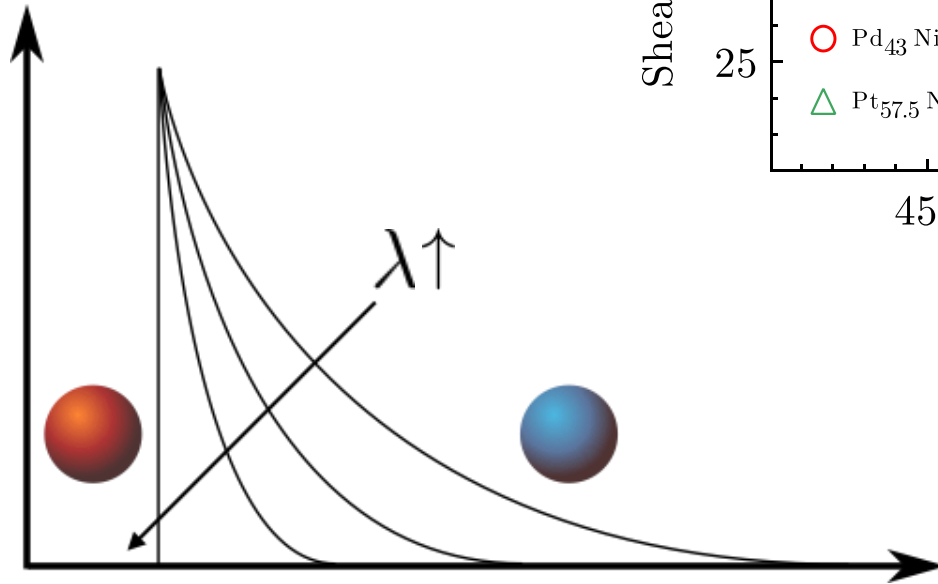
Yielding of colloidal glasses: comparing with confocal microscopy (2)



Comparison with experimental data: metallic glass (1)

Apply model to real world:

Rheological measurements for
metallic glass alloys (ultra-
sonic)



$\Rightarrow \lambda$ controls the **slope** of
the shear modulus

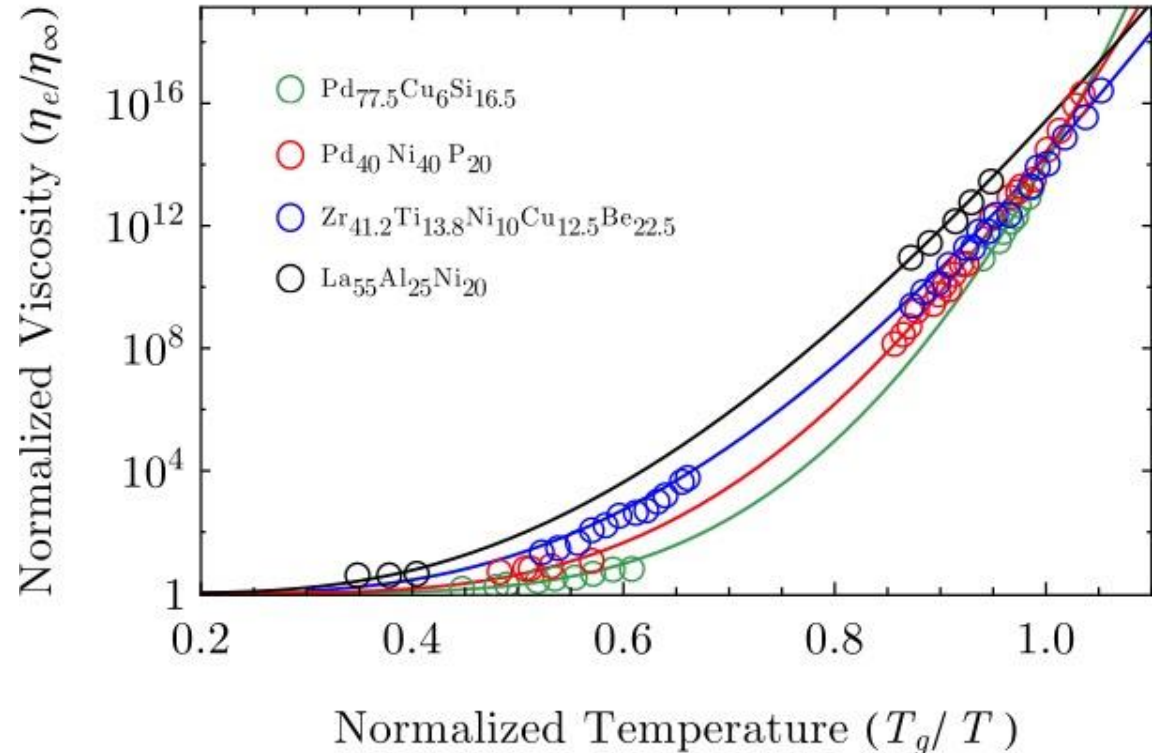
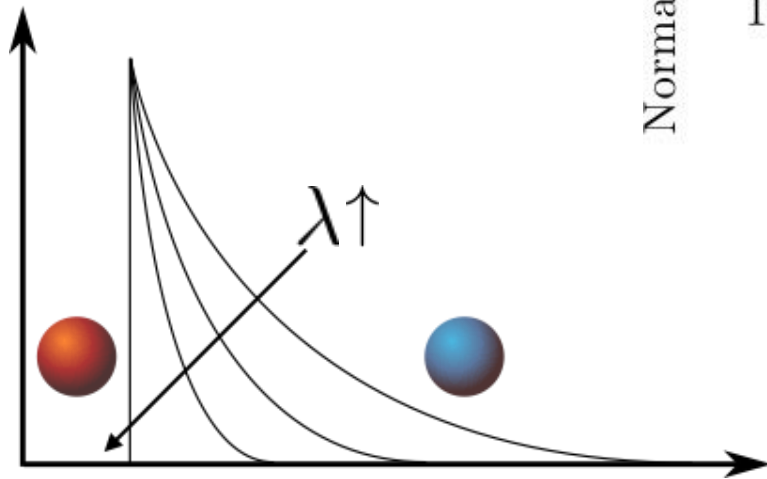
Johnson et. al, MRS Bull. (2007)

Krausser, Samwer, Zaccone, PNAS (with referees)

Comparison with experimental data: metallic glass (2)

Definition of **fragility**:

$$m = \left. \frac{\partial \log(\eta/\eta_0)}{\partial (T_g/T)} \right|_{T=T_g}$$



$$m(\lambda) = \frac{V_c C_G}{k_B T_g} [1 + (2 + \lambda) \alpha_T T_g]$$

Johnson et. al, MRS Bull. (2007)

Krausser, Samwer, Zaccone, PNAS (with referees)

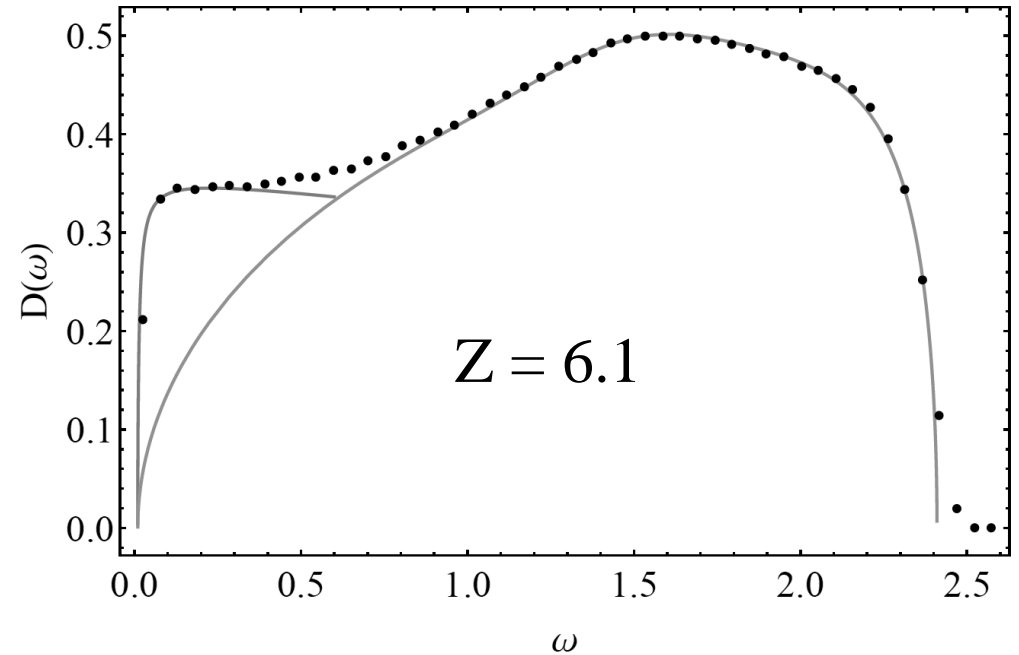
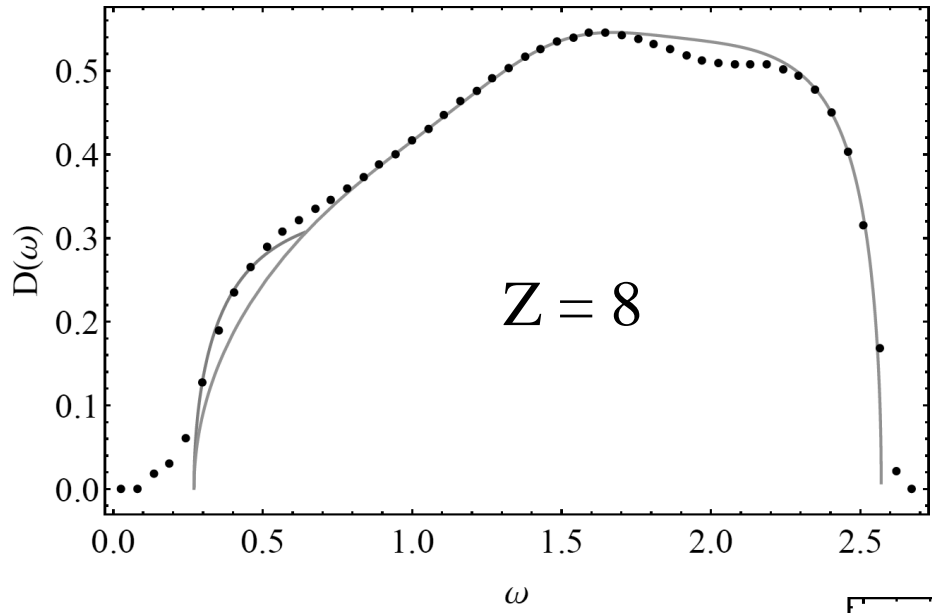
Parameters for overshoot fitting

$K[18]$ (GPa)	$\eta[18]$ (GPa s)	τ_c (s)	τ_v (s)	$T[18]$ (K)
12	80	1.6	2.13	523
3.6	12	1.6	0.32	643
1.2	4	0.6	0.12	663
0.6	2	0.01	0.053	685
$K[18]$ (GPa)	$\eta[18]$ (GPa s)	τ_c (s)	τ_v (s)	$\dot{\gamma}[18]$ (s ⁻¹)
3.6	80	12	9.0	2×10^{-4}
3.6	80	12	7.3	5×10^{-3}
3.6	22	1.8	0.32	0.032
3.6	12	1.6	0.12	0.10

COMPARISON WITH ALTERNATIVE THEORIES

- **MCT** with shear: 5-6 free parameters. Shear parameters c_γ and λ have no clear physical meaning (cfr. discussion in Binder & Kob's book).
- **STZ** theory: ~4 parameters (effective T not well-defined)

Vibrational DOS from random matrix theory



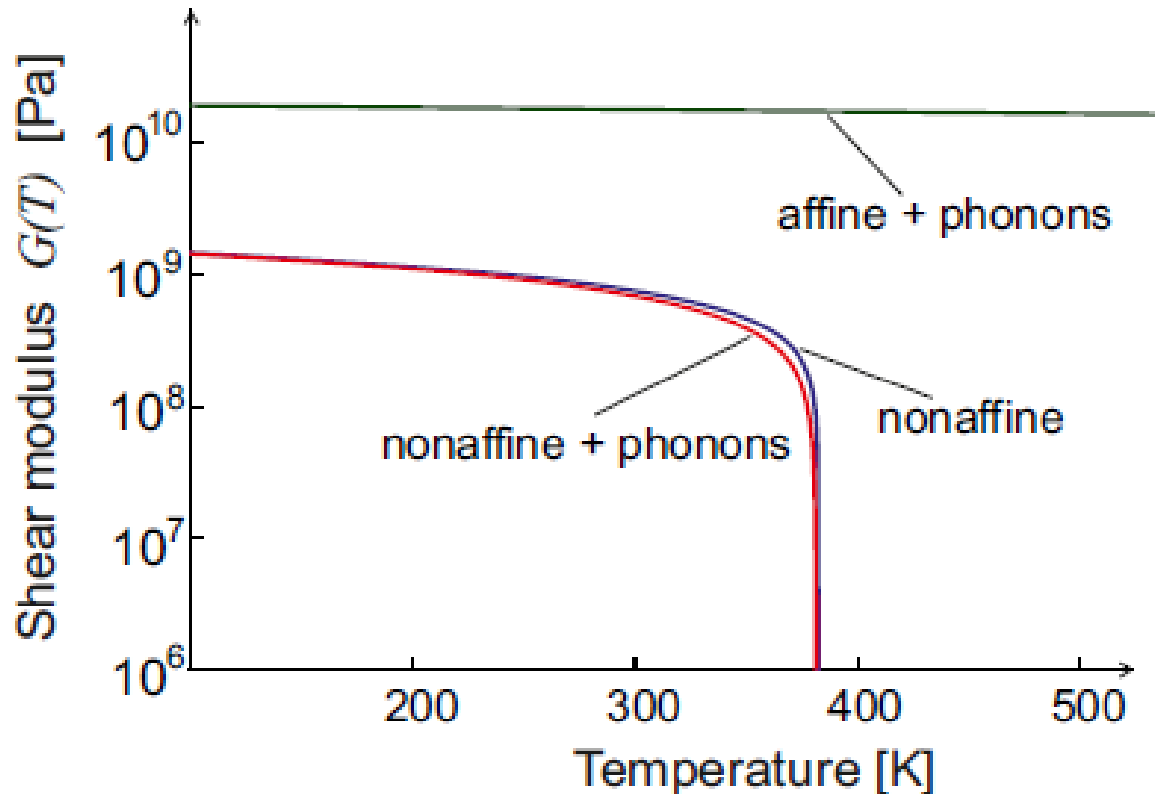
Av. number of contacts z decreases with $T \uparrow$

We found: $G \approx \frac{N}{V} \kappa r_0^2 (z - z_c) \quad \longrightarrow \quad G \approx \frac{\kappa}{r_0} \phi_c e^{\alpha(T_c - T)} \sqrt{\phi_c [e^{\alpha(T_c - T)} - 1]}$

There is one more contribution for the $G(T)$: from **phonon modes** that shift their characteristic frequency on deformation
[J. Frenkel 1946]

$$G_{\text{phonons}} \approx -\frac{k_B T}{r_o^3} e^{-\alpha T}$$

...but it turns out to be small

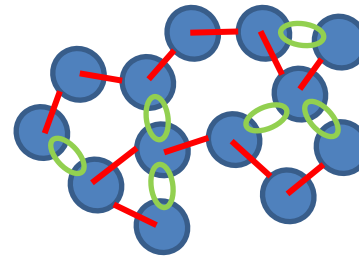


May be we can find Tg from G→0 ?

We now know: $G \approx \frac{\kappa}{r_0} \phi_c e^{\alpha(T_c - T)} \sqrt{\phi_c [e^{\alpha(T_c - T)} - 1]}$

because

$$(z - z_c) \sim \sqrt{\phi - \phi_c}$$



To formulate all this in a 'normal language'

1. In order to be a rigid glass, the system has to have $z_{VDW} \geq 12 - 5z_{CO}$ additional physical LJ bonds.
2. In a long polymer chain $z_{CO} \approx 2$ and so there should be at least $z_{VDW} \approx 2$ of extra contacts per monomer.

The critical point $\phi_c = e^{-\alpha_T T_g + C}$

is related to $z_{CO} = 2 - 2/n$

Via $\phi_c = \phi_c^0 - \Lambda \cdot z_{CO}$

└──────────┴──────────┘ ~0.64

...which solves for Tg

Fox and Flory, 1950

Expanding the exponential to linear order:

$$T_g \approx \frac{1}{\alpha_T} \left(1 + C - \phi_c^0 + 2\Lambda \right) - \frac{2\Lambda}{\alpha_T n}$$



$\Lambda \sim 0.1$ from experiment
 $C = 0.48$ to give Tg=383K
 $\phi = 0.61 e^{-\alpha_T T}$

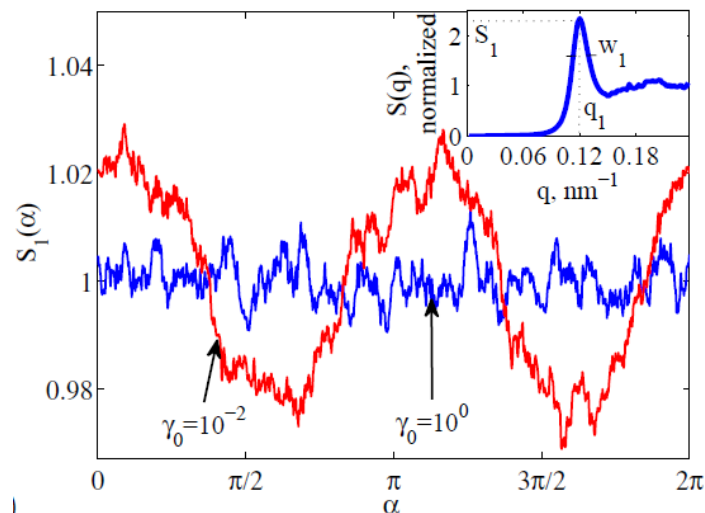
Cage distortion and yielding of colloidal glasses

Theory predicts **p-wave** symmetry distortion in the plane beneath shear plane which vanishes at yielding (fully nonaffine response after yielding)

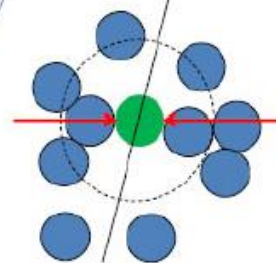
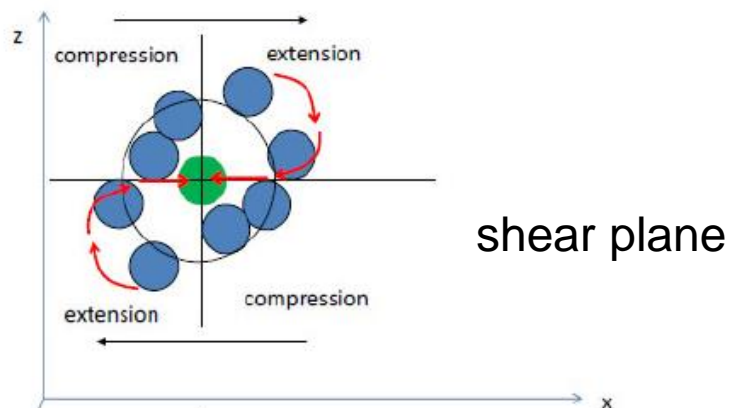
$$\mathbf{u}(\mathbf{r}) = -\frac{p}{4\pi K} \frac{\mathbf{r} \cdot \mathbf{n}}{r^3} \mathbf{n} \quad \text{dipole field}$$

$$u(\alpha) \propto \mathbf{r} \cdot \mathbf{n} \propto \sin^2 \theta \cos^2 \alpha = \cos^2 \alpha$$

p-wave symmetry in the experimental angular correlation function (colloidal glass):

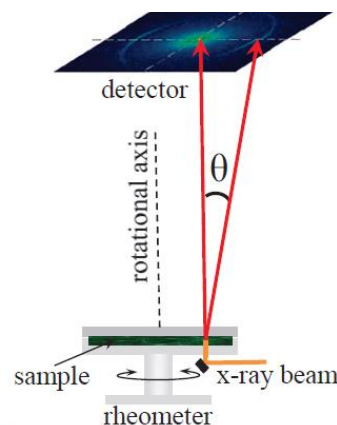


PREDICTION VERIFIED!



shear plane

plane where scattering is measured

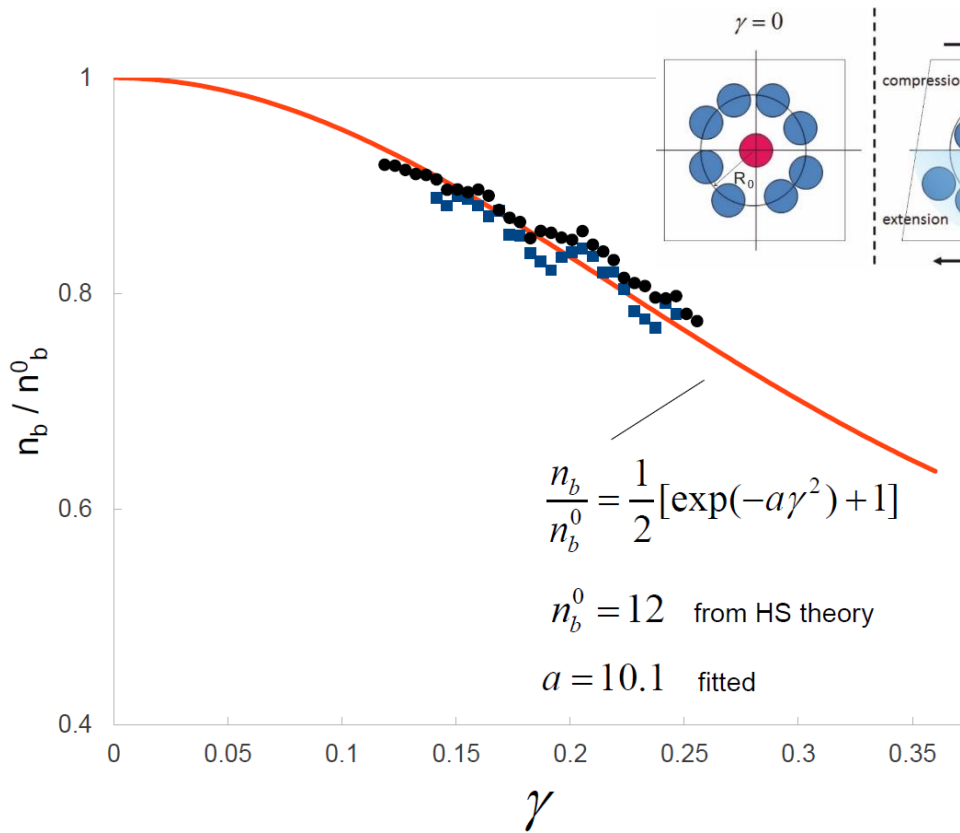


angle-resolved **rheo-SAXS** (Desy-Hamburg)

coll. with **Peter Schall (Amsterdam)**

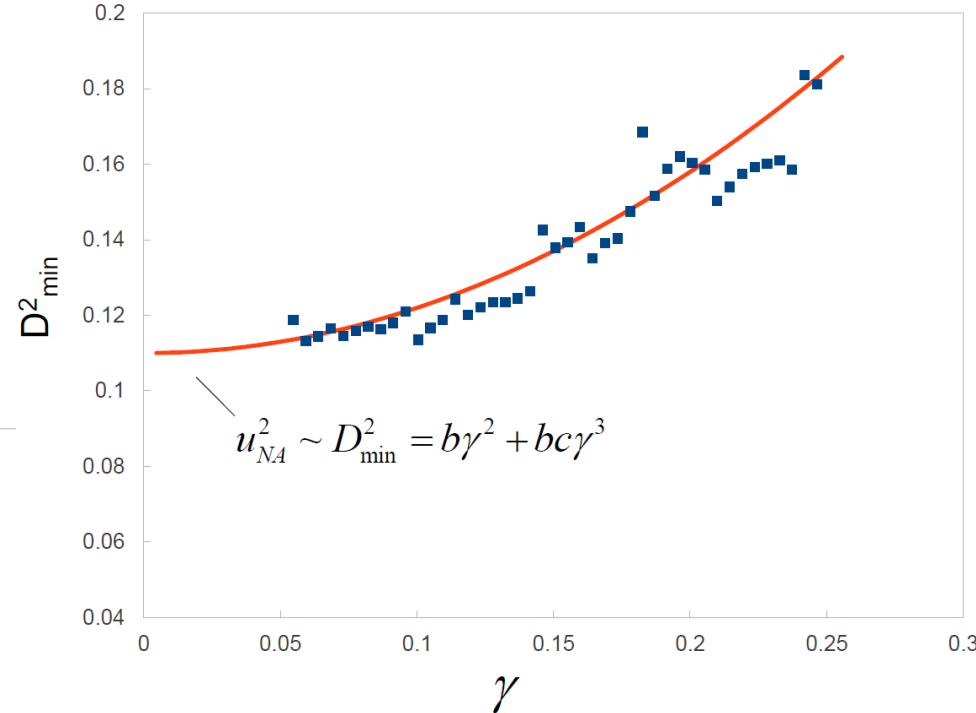
Yielding of colloidal glasses:

Direct relation between nonaffine displacements and stress-strain relation



Strain-induced loss of **permanent** nearest-neighbours

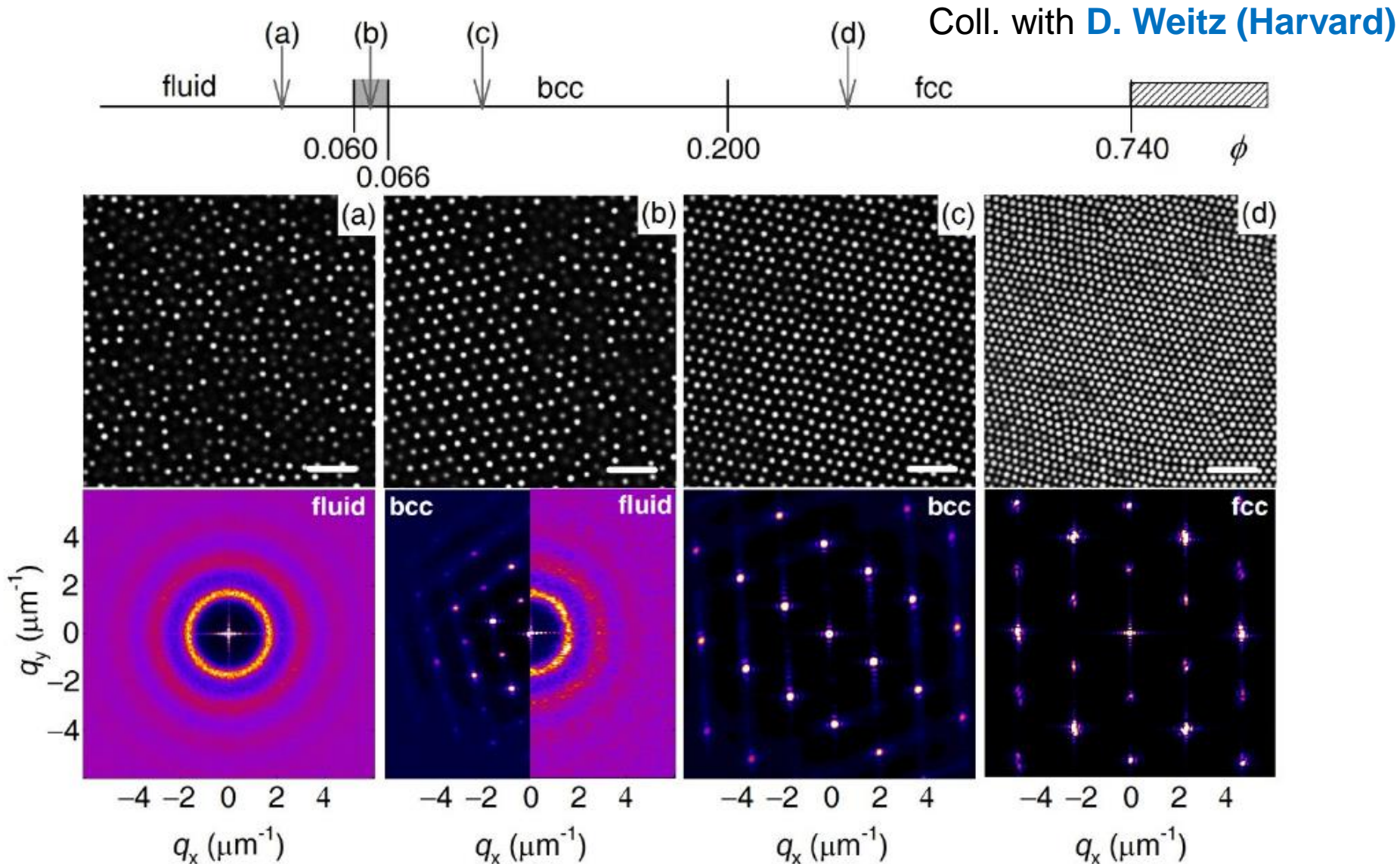
Mean-squared nonaffine displacements



Experimental data from confocal microscopy (S. Egelhaaf & M. Laurati)

Application: colloidal crystal melting in 3D

Colloidal crystals: the particles (~ 1 micron) and their dynamics can be followed by confocal microscopy (unlike atoms)

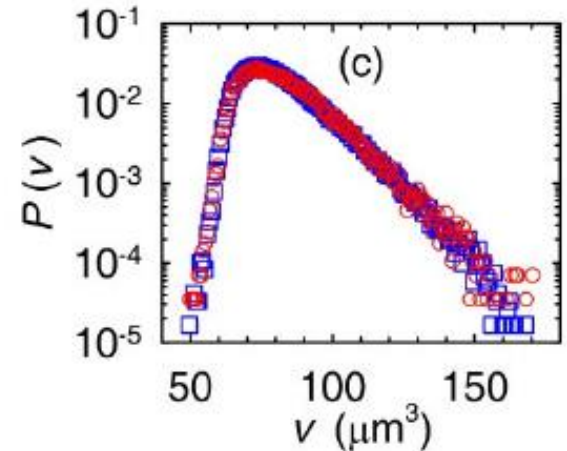
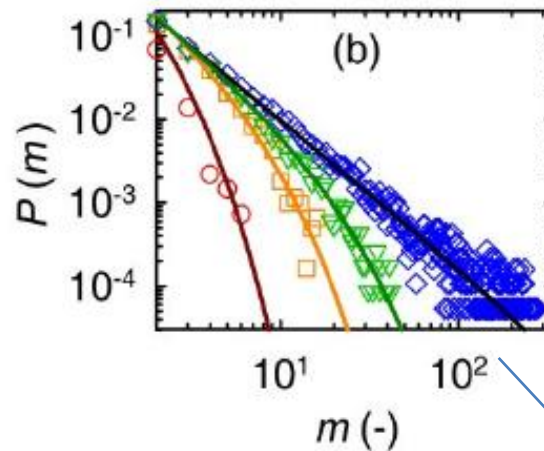
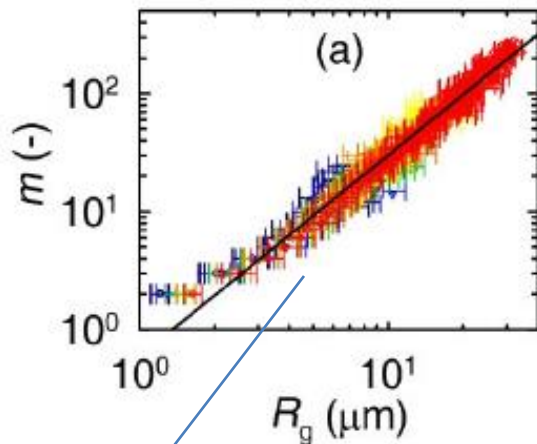
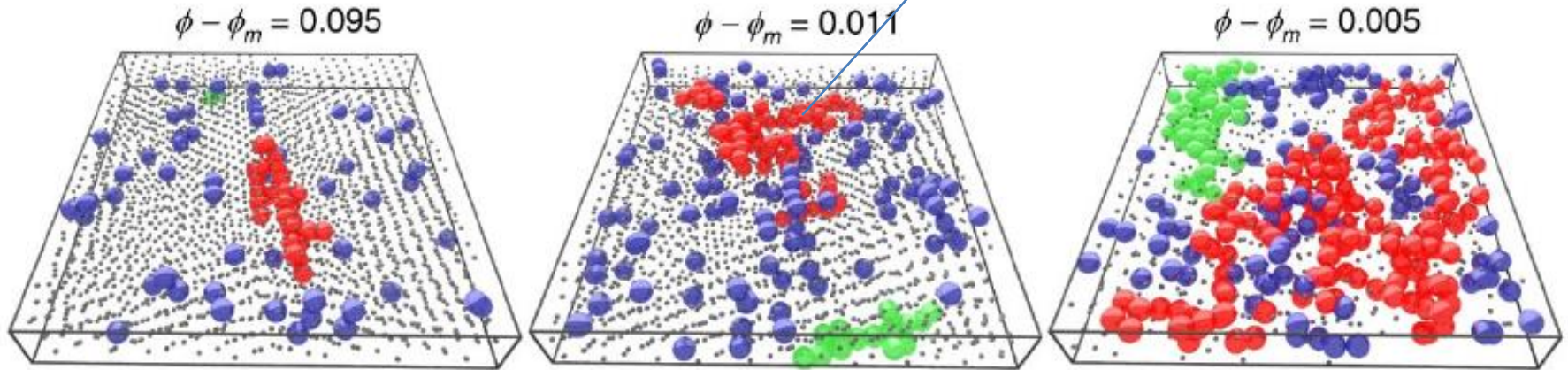


Strong thermal disorder: fluctuations

With colloids, melting is driven by the density ϕ . Upon approaching the melting point, the dynamics of particles becomes highly **disordered** (thermal fluctuations)

Sprakel, Zaccane, Spaepen, Schall, Weitz, preprint 2014

clusters of highly mobile particles



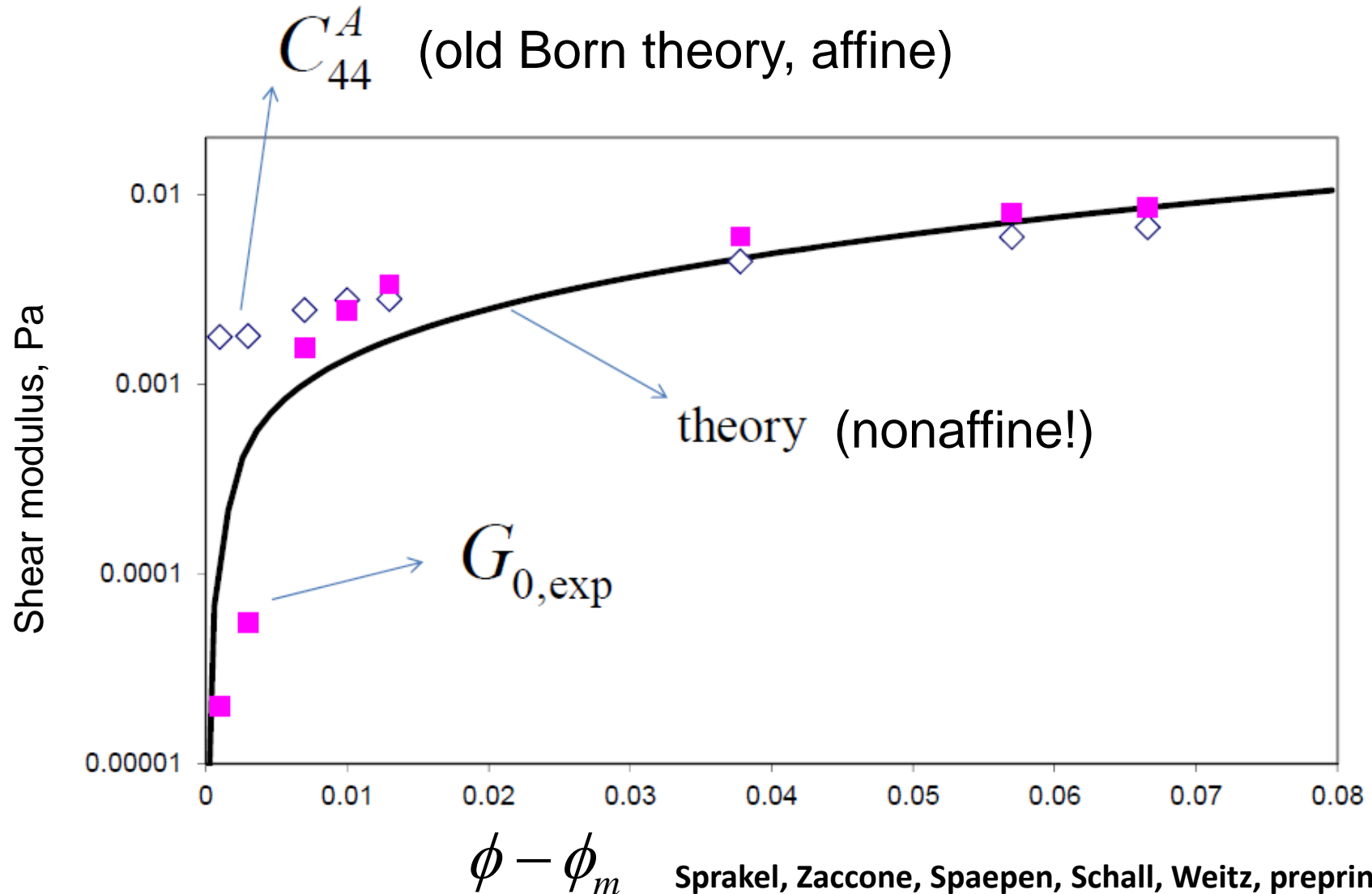
fractal dimension of the clusters ~ 1.75

critical exponents

A new melting criterion

Born criterion (1939): crystals melt when the affine shear modulus vanishes

Our new criterion: crystals melt when the **nonaffine** shear modulus vanishes, due to thermal fluctuations!



Overview – disordered materials

**Nonaffine theory
of amorphous materials
can explain and describe**

The difference in **material strength**
between crystals and glasses

The **glass transition** and
mechanical properties
of **glassy polymers**

The mechanical failure
of **metallic glasses** under strain

The **solid-liquid tr. of 3D crystals with no defects**

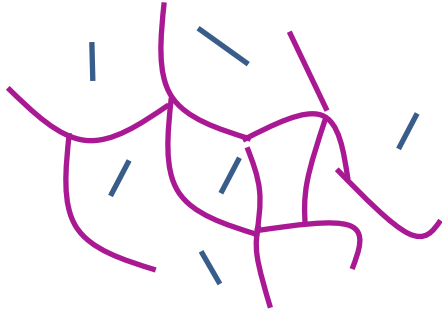
The link between **interatomic potential**
and the **fragility** of **metallic glasses**

21st century materials: a “disordered” revolution

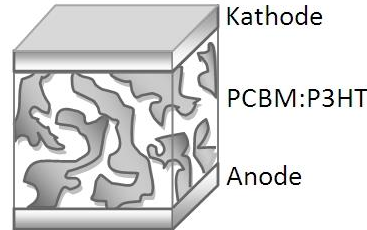
SOFT



HARD

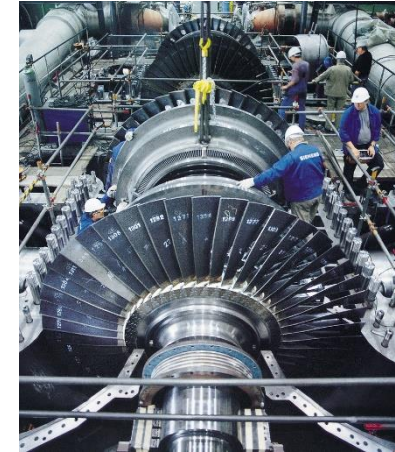


hydrogels
(tissues, drug-delivery
foods, cosmetics...)

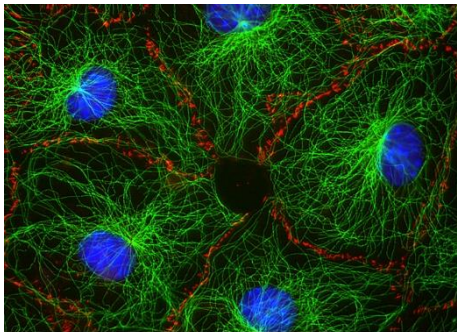


solar cells

AZ
Research Group



superalloys
metallic glasses



cells' cytoskeleton

PhD Students:

J. Krausser

R. Milkus

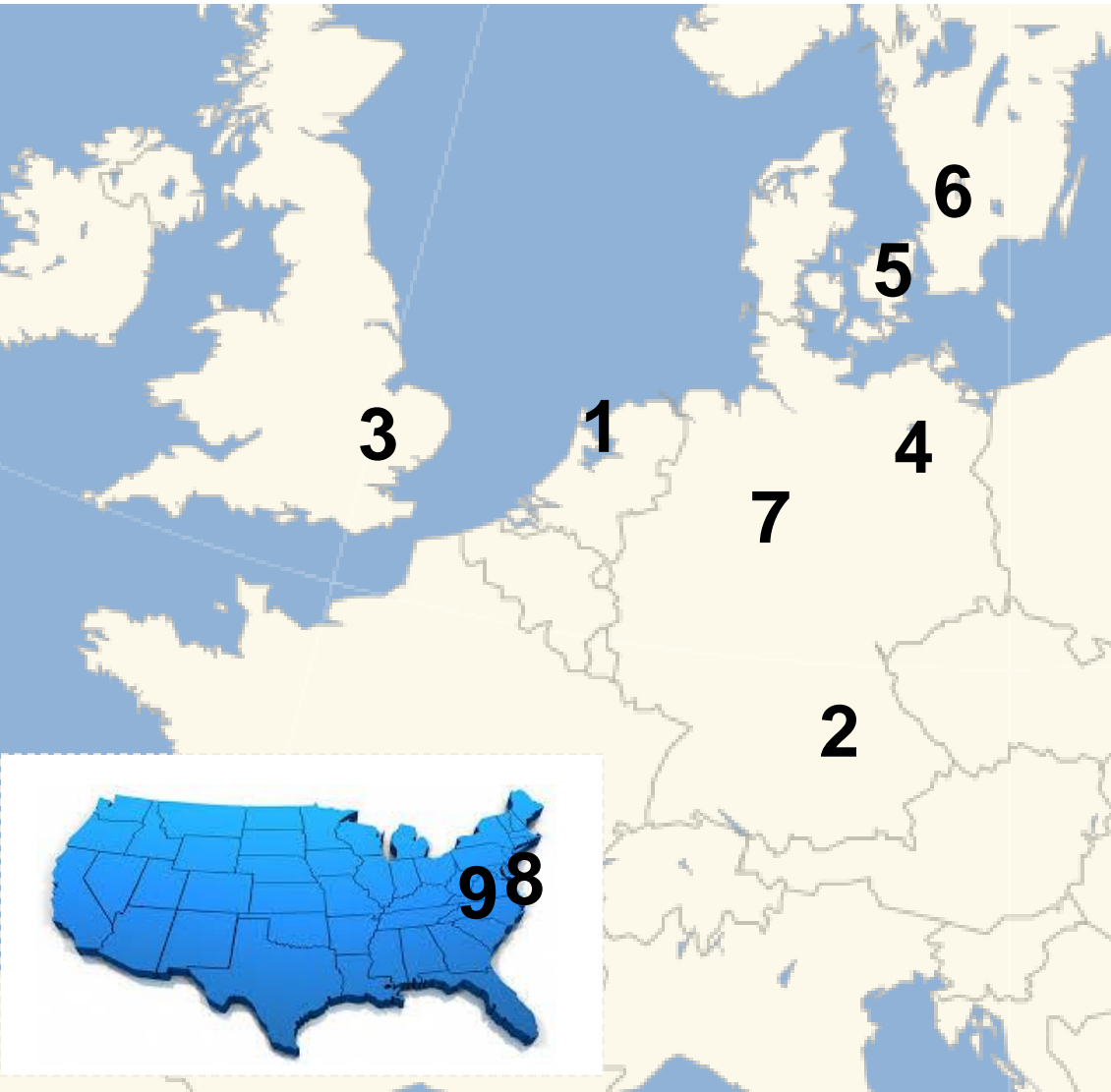
Post-Docs (from 03.15):

M. Abnekar

H. Yamani



Experimental collaborators



1. Amsterdam

Glasses, shear-banding

- P. Schall, D. Bonn

2. Munich Bio-nanoaggregates

- P. Muller-Buschbaum

- A. Bausch

3. Cambridge Gels, proteins

- T. Knowles

- P. Cicuta, E. M. Terentjev

4. Berlin Gels, nanoparticles

- M. Ballauff

5. Copenhagen + 6. Lund

Proteins

- B. Vestergaard

- P. Schurtenberger

7. Goettingen Metals

- K. Samwer

8. Harvard

Glasses, Metallic alloys

- D. Weitz, F. Spaepen

9. Amherst Gels

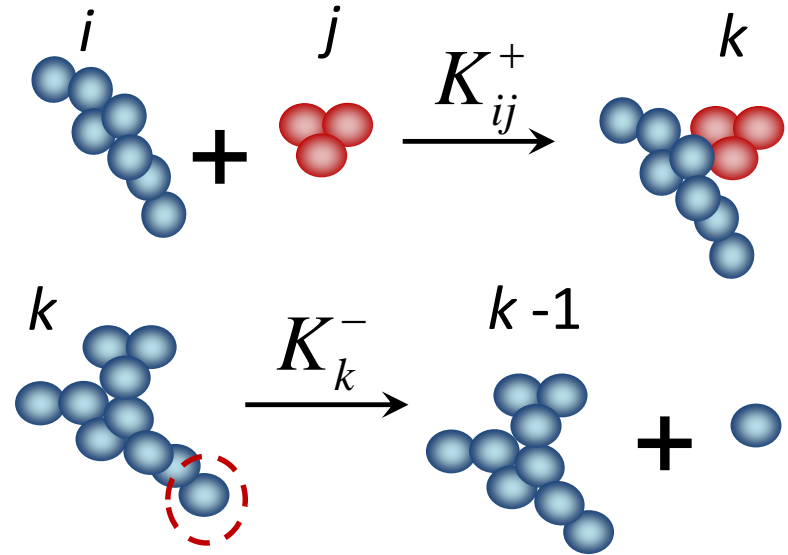
- H.H. Winter

Mathematical approach: master kinetic equation

Until now: equilibrium statistical mechanics (Flory-Stockmayer, AHS, percolation), no time-evolution, cannot link molecular level with macroscopic structure & properties

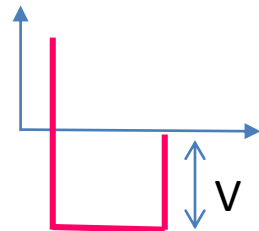
NEW APPROACH: master kinetic equations (**NONEQUILIBRIUM!**)

$$\frac{dc_k}{dt} = \frac{1}{2} \sum_{i,j=1}^{i+j=k} K_{ij}^+ c_i c_j - c_k \sum_{i=1}^{\infty} K_{ik}^+ c_i - K_k^- c_k + \sum_{i=k+1}^{\infty} K_{ik}^- c_i$$



K_{ij}^+ assembly rate  diffusion-limited (Smoluchowski)

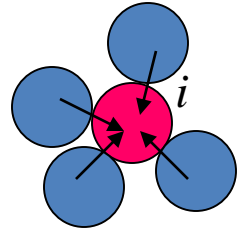
K_k^- disassembly rate  Arrhenius-Kramers dependence on bond energy



Free energy of lattice deformation with disorder

$$W = \mathcal{F}_{NA} = \int_0^{u^{NA}} \delta \underline{f}_i \cdot d\underline{x}_i = -\frac{1}{2} \underline{\underline{H}}_{ij} u_i^{NA} u_j^{NA}$$

$$= -\frac{1}{2} \left(\underline{\Xi}_i \cdot \frac{\partial \underline{r}_i}{\partial \gamma} \right) \gamma^2$$



$$\underline{\underline{H}}_{ij} \frac{\partial \underline{r}_j}{\partial \gamma} \Big|_{\gamma \rightarrow 0} = \underline{\Xi}_i$$

internal work done by nonaffine motions
at the expense of lattice energy of deformation

~ force acting on i
due to affine motions
of j neighbours

Zaccone & Scossa-Romano, PRB (2011)

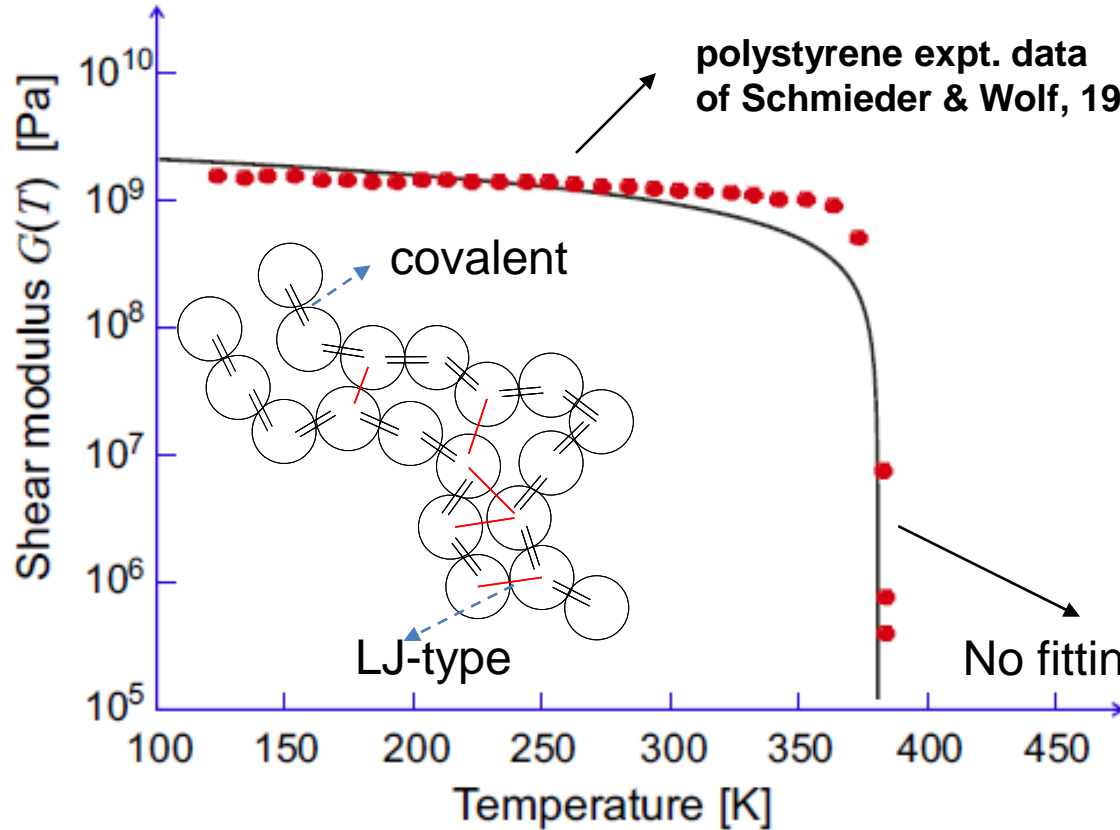
$$\mathcal{F} = \mathcal{F}_A - \mathcal{F}_{NA} = \mathcal{F}_A - \frac{1}{2} \left(\underline{\Xi}_i \cdot \frac{\partial \underline{r}_i}{\partial \gamma} \right) \gamma^2$$

affine, "ordered"

nonaffine, "disordered"

Application (1): polymer glass transition

$$F = F_A - F_{NA} - F_T \rightarrow \text{phonons also contribute to the elastic free energy}$$



No theories available for G at $T < T_g$

At $T > T_g$:
Doi-Edwards theory, tube theory

No fitting parameters!

Zaccone & Terentjev, PRL 2013

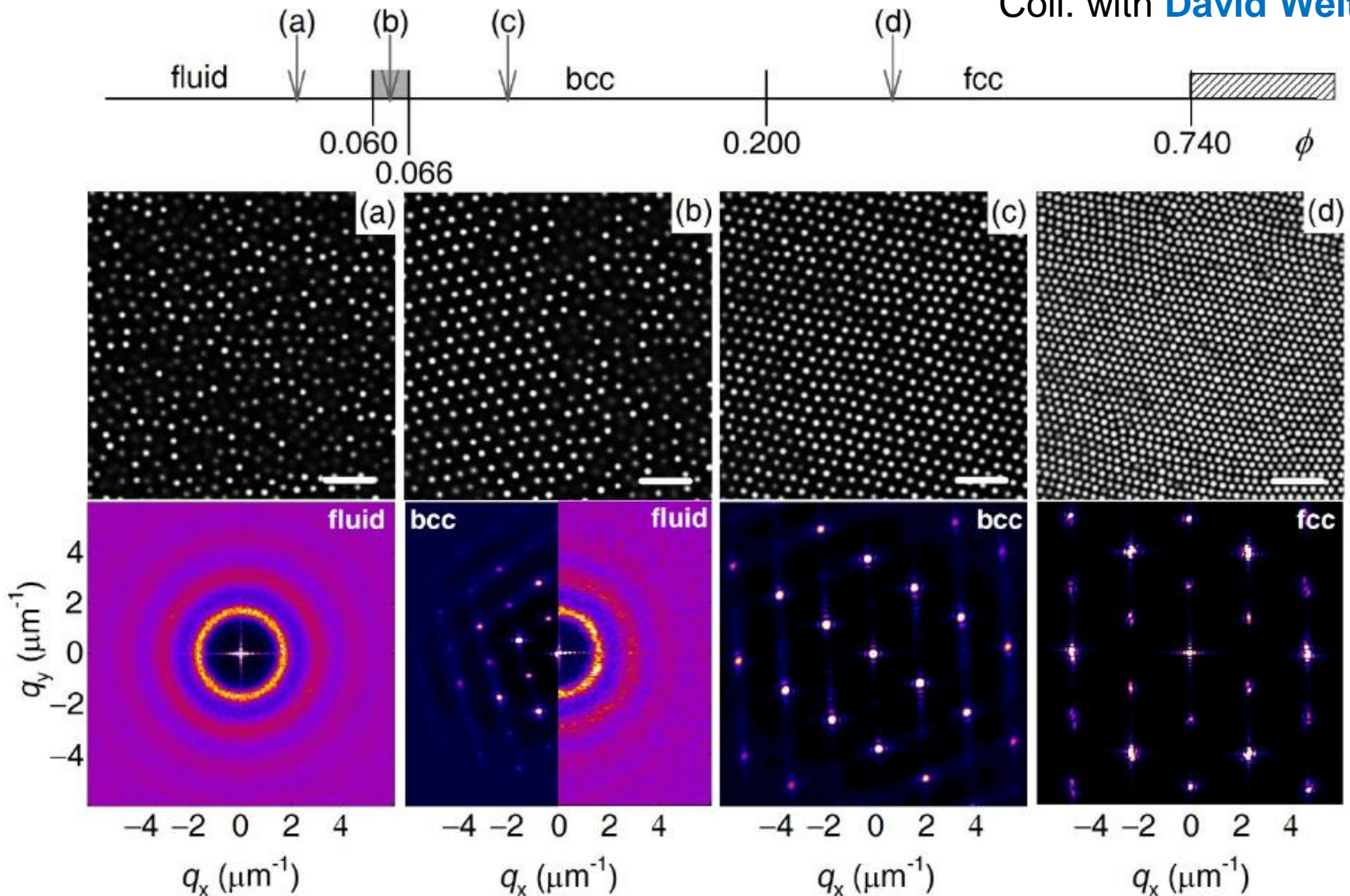
$$G = \frac{2}{5\pi} \left(\frac{\kappa}{R_0} \phi_c e^{\alpha_T(T_c - T)} \sqrt{\phi_c [e^{\alpha_T(T_c - T)} - 1] - \frac{kT}{R_0^3} e^{-\alpha_T T}} \right) \sim \sqrt{T_c - T}$$

scaling confirmed by MD simulations in J. Wittmer et al., JCP 2013

Application (2): crystal melting in 3D

Colloidal crystals: the particles (~ 1 micron) and their dynamics can be followed by confocal microscopy (unlike atoms)

Coll. with **David Weitz**

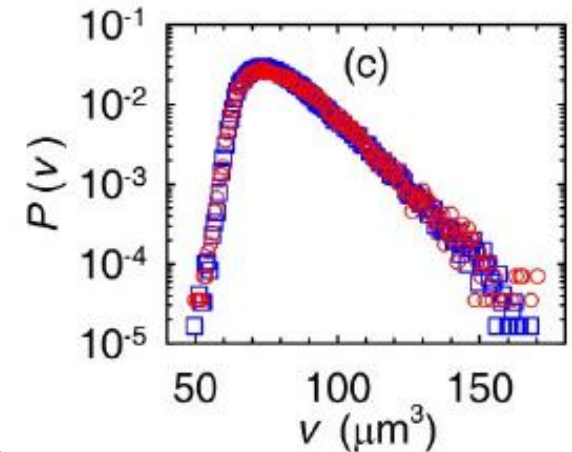
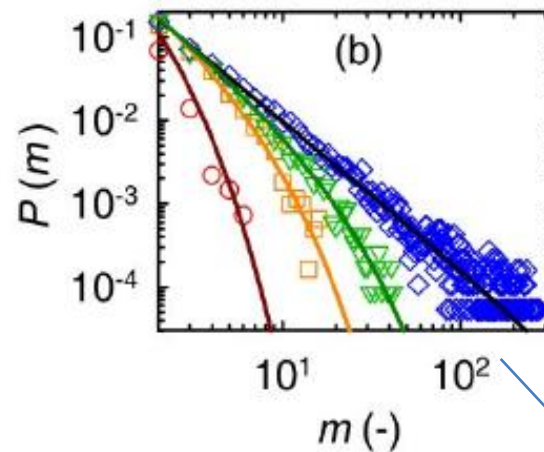
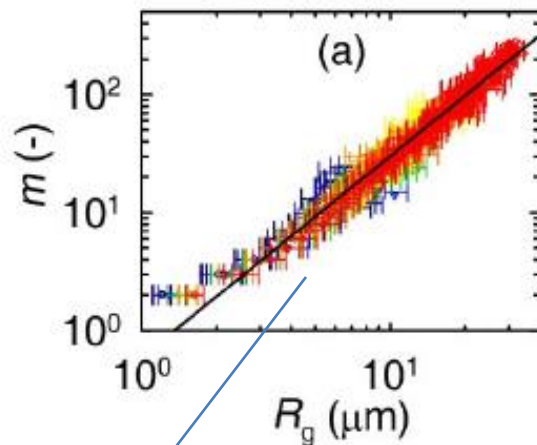
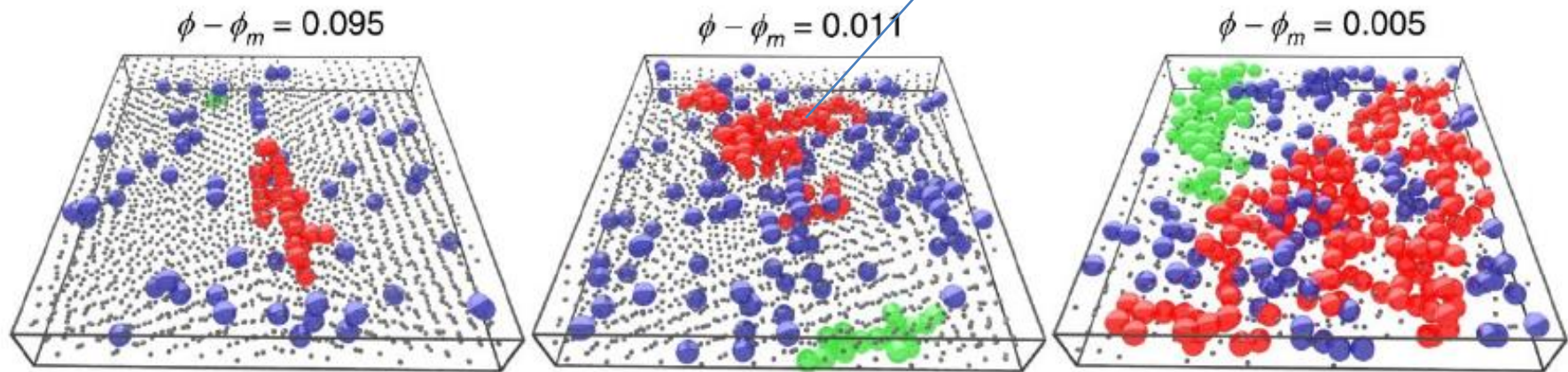


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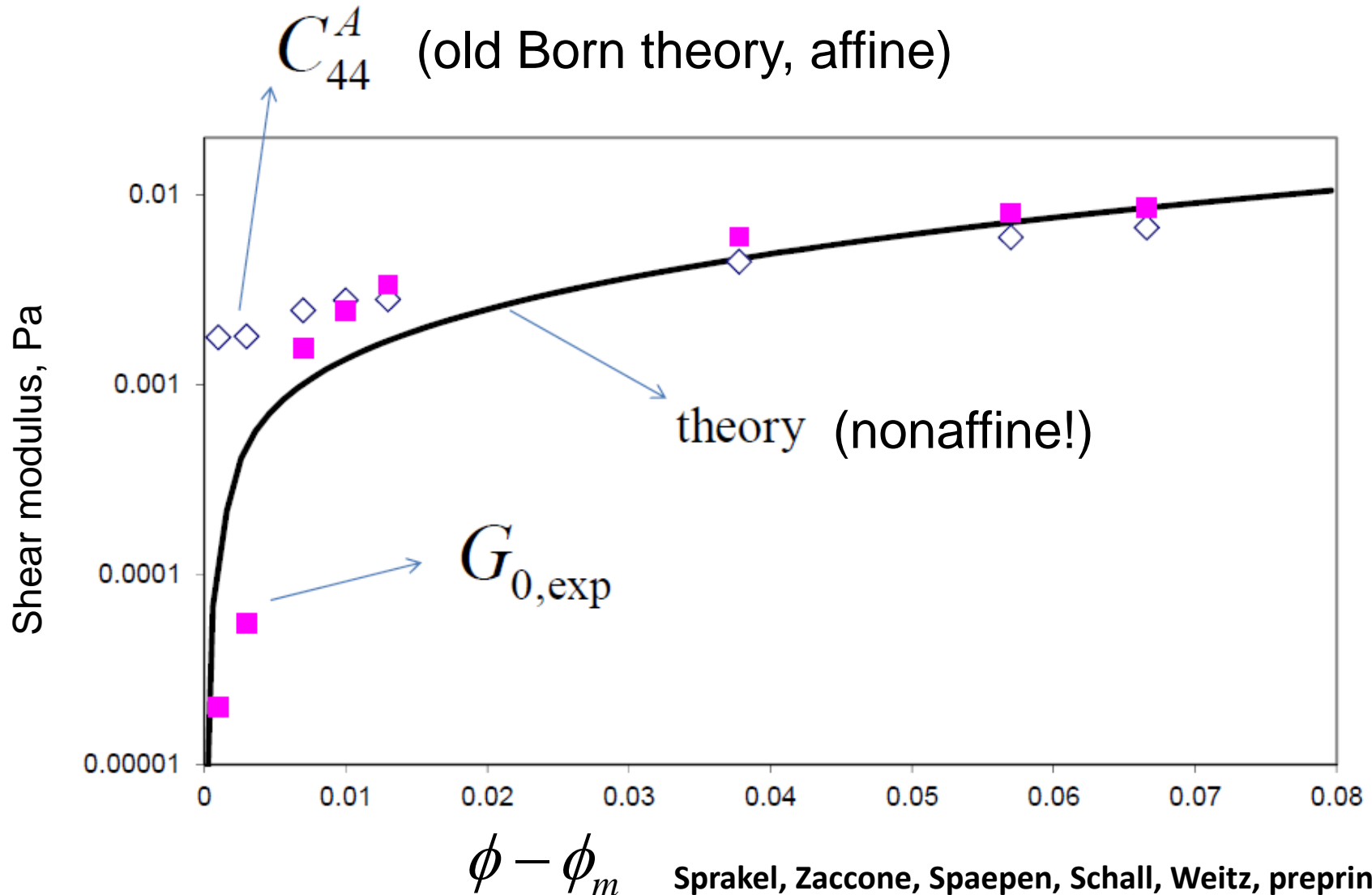
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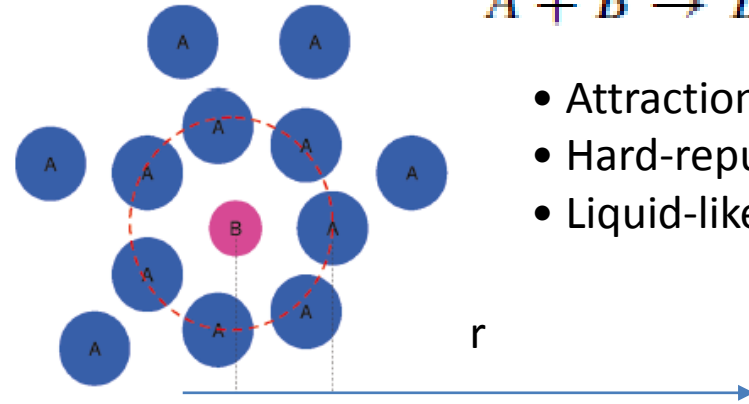


Bimolecular association reactions in crowded environments

Dorsaz et al. PRL 105, 120601 (2010)



- Attraction between A and B
- Hard-repulsion among A's
- Liquid-like structure



How does the association rate depend on the crowding packing fraction?

Governing equation (Smoluchowski diff. eq.)

$$\frac{\partial \rho}{\partial t} = D_c \nabla \cdot (\nabla \rho - \beta F \rho).$$

collective diff.

effective force-field due to crowders:

$$-\int \beta F dr = \beta \int \frac{1}{\rho} \frac{d\Pi}{dr} dr = \beta \int \frac{1}{\rho} d\Pi \rightarrow \text{changes with } r \text{ due to } g(r) !$$

