Effective thermodynamics for a system with dry friction

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STATISTICAL MECHANICS OF FRICTIONAL ATHERMAL SYSTEMS ?



Edwards All packings where grains occupy the same volume are equiprobable

Frictional grains: change of configurations due to "extensive operations"

$$S \sim \log \int d\mathbf{q} \ \delta(V - \mathcal{W}(\mathbf{q}))$$

S.F Edwards, C.C. Mounfield, Physica A (210), 1994



$$\frac{1}{T} = \frac{\partial S}{\partial E} \implies \frac{1}{X} = \frac{\partial S}{\partial V}$$

Compactivity

TEST OF EDWARDS ASSUMPTION



 \mathcal{C}_1



Dissipation



 \mathcal{C}_2

Energy injection through vertical vibration of the box (tapping)

Average over states collected via tapping

$\langle \mathcal{O} \rangle_{\text{emp},V} = \mathcal{N}^{-1} \sum_{i} \mathcal{O}(\mathcal{C}_{i}) \ \delta(V - W(\mathcal{C}_{i}))$

THERMODYNAMIC SAMPLING

Thermodynamic average with Edwards measure

$$\langle \mathcal{O} \rangle_X = \mathcal{Z}^{-1} \sum \mathcal{O}(\mathcal{C}) \ e^{-W(\mathcal{C})/X}$$

AMORPHOUS PACKINGS & GLASSES

Number of blocked structures in frictional granular assemblies at given Volume

Number of energy minima in models of glasses at given Energy

 $\log[\mathcal{N}_{blocked}(V)] \sim N$

 $\log[\mathcal{N}_{\min}(E)] \sim N$

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Edwards' Measures for Powders and Glasses

Alain Barrat,¹ Jorge Kurchan,² Vittorio Loreto,³ and Mauro Sellitto⁴

A statistical mechanics approach to the inherent states of granular media

Antonio Coniglio^{a,*}, Mario Nicodemi^{a,b}

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Possible Test of the Thermodynamic Approach to Granular Media

David S. Dean and Alexandre Lefèvre





A. Lefèvre & D. Dean, J. Phys. A: Math. Gen. 34 (2001)

TAPPING DYNAMICS

"BLOCKED CONFIGURATIONS"

1) Heating: all spins are flipped with probability $\ p \in [0, 1/2[$

2) Quench at T=0: only spin flips which lower the energy are allowed

Energy cannot be lowered with a single spin flip

Heating
$$\rightarrow$$
 Quench T=0 \rightarrow Heating \rightarrow Quench T=0 \rightarrow E_2

$$\mathcal{Z} = \sum_{\boldsymbol{\sigma}} e^{\beta_{Ed} \sum_{i} \sigma_{i} \sigma_{i+1}} \prod_{i} \Theta(\sigma_{i-1}\sigma_{i} + \sigma_{i}\sigma_{i+1}) \quad \begin{array}{l} x \ge 0 \ \to \ \Theta(x) = 1 \\ x < 0 \ \to \ \Theta(x) = 0 \end{array}$$

Edwards measure $\langle \mathcal{O} \rangle_E = \mathcal{Z}^{-1} \sum_{\{\boldsymbol{\sigma} | \boldsymbol{\sigma} \in \text{blocked}\}} \mathcal{O}(\boldsymbol{\sigma}) \ e^{-\beta_{Ed} E(\boldsymbol{\sigma})}$



J. Berg, S. Franz, M. Sellitto, EPJ B (2002)

- Same test on a different 1D spin model (Friedrickson-Andersen)
- Disagreement between dynamical averages and Edwards effective theory

HARMONIC CHAIN WITH DRY FRICTION



HARMONIC CHAIN WITH DRY (Coulomb) FRICTION



TAPPING DYNAMICS

1) External force switched on for a fixed duration τ : energy injection

$$m \ddot{x}_{i} = -mg\mu_{d} \operatorname{sgn}(\dot{x}_{i}) + (x_{i+1} + x_{i-1} - 2x_{i}) + F n_{i}$$

$$p(n_{i}) = (1 - \rho) \,\delta(n_{i}) + \rho \,\delta(1 - n_{i})$$

Annealed disorder: for each "tap" the particles pulled are different

2) External force **<u>switched off</u>**: relaxation to mechanically stable (blocked) configuration, all particles are at rest

$$m \ddot{x}_i = -mg\mu_d \operatorname{sgn}(\dot{x}_i) + (x_{i+1} + x_{i-1} - 2x_i)$$

Dynamics is arrested

$$\dot{x}_i = 0 \quad \forall i$$
$$|x_{i+1} + x_{i-1} - 2x_i| < \mu mg$$

$$e = \frac{1}{N} \sum_{i=1}^{N} \frac{\xi_i^2}{2}$$

Energy of the mechanically stable configurations

 $\xi_i = x_i - x_{i-1} - \ell_0$ Spring elongation

HARMONIC CHAIN WITH DRY (Coulomb) FRICTION



SPRING-SPRING CORRELATION (IN MECHANICALLY STABLE CONFIGURATIONS)



 $\langle \xi_m \xi_n \rangle_{\mathrm{emp},F}$

 $\langle \xi_m \xi_n \rangle \sim C(|n-m|/\ell(e))$



the "tapping" dynamics we used

EFFECTIVE THERMODYNAMICS "Á LA EDWARDS"

"Given a certain situation attained dynamically, physical observables are obtained by averaging over the *usual equilibrium distribution* at the corresponding volume, energy, etc. but restricting the sum to 'blocked' configurations." (Barrat, Kurchan, Loreto, Sellitto)

$$oldsymbol{\xi} = \{\xi_1, \dots, \xi_N\}$$
 Springs elongations

$$\mathcal{Z} = \int \mathcal{D}\boldsymbol{\xi} \ e^{-\beta_{Ed}E[\boldsymbol{\xi}]} \ \delta[\mathcal{F}(\boldsymbol{\xi}) - 1]$$

Mechanical stability $\mathcal{F}(\boldsymbol{\xi}) = 1$

Otherwise $\mathcal{F}(\boldsymbol{\xi})=0$

$$E[\boldsymbol{\xi}] = \sum_{i=1}^{N} \frac{\xi_i^2}{2} \qquad \beta_{Ed} = \left[\frac{\partial S}{\partial E}\right]_{\mathcal{F}(\boldsymbol{\xi})=1}$$

EFFECTIVE THERMODYNAMICS "Á LA EDWARDS"



$$\mathcal{Z} = \int d\xi_1 \dots d\xi_N \ e^{-\beta_{Ed} \sum_{i=1}^N \frac{\xi_i^2}{2}} \prod_{i=1}^N \Theta(\mu - |\xi_{i+1} - \xi_i|)$$
$$\mathcal{Z} = \int d\xi_1 \dots d\xi_N \ \prod_{i=1}^N T(\xi_i, \xi_{i+1})$$

$$T(x,y) = e^{-\beta_{Ed}\frac{x^2}{4}}\Theta(\mu - |x - y|)e^{-\beta_{Ed}\frac{y^2}{4}} \quad x \ge 0 \to \Theta(x) = 1$$
$$x < 0 \to \Theta(x) = 0$$

Transfer Operator Formalism

$$\mathcal{T}[f](x) = \int_{-\infty}^{\infty} dy \ T(y, x) f(x)$$

$$\mathcal{Z} = \operatorname{Tr}[\mathcal{T}^N]$$

"THERMODYNAMIC" POTENTIALS

$$T(x,y) = e^{-\beta_{Ed} \frac{x^2}{4}} \Theta(\mu - |x - y|) e^{-\beta_{Ed} \frac{y^2}{4}}$$

 $T(x,y) \in L^2(X \ge Y)$

Hilbert-Schmidt integral operator maximum isolated eigenvalue

$$\mathcal{Z} = \operatorname{Tr}[\mathcal{T}^N]$$

$$f(\beta_{Ed},\mu) = -\frac{1}{\beta_{Ed}} \log[\lambda_{\max}(\beta_{Ed},\mu)]$$

$$e = \partial_{\beta_{Ed}}(\beta_{Ed}f)$$

$$e = -\lambda_{\max}^{-1} \langle \lambda_{\max} | \partial_{\beta_{Ed}} \mathcal{T} | \lambda_{\max} \rangle$$

"THERMODYNAMIC" POTENTIALS

$$T(x,y) = e^{-\beta_{Ed} \frac{x^2}{4}} \Theta(\mu - |x - y|) e^{-\beta_{Ed} \frac{y^2}{4}}$$



"THERMODYNAMIC" POTENTIALS



SPRING-SPRING CORRELATION FUNCTION

The operator (real, symmetric kernel) has an orthonormal basis

$$\mathcal{T}[f_b](x) = \lambda_b f_b(x) \qquad \int_{-\infty}^{\infty} f_b(x) f_a(x) = \delta_{a,b}$$

$$\lim_{N \to \infty} \langle \xi_m \xi_n \rangle_{Ed} = \sum_{b \in Sp(\mathcal{T})} \left(\frac{\lambda_b}{\lambda_{\max}} \right)^{n-m} \left| \int_{-\infty}^{\infty} dx \ x f_b(x) f_{\lambda_{\max}}(x) \right|^2$$
Points = effective thermodynamics Lines = tapping dynamics (p=0.3)
Comparison is at fixed energy

CORRELATION FUNCTION $C(|n-m|) \sim \exp(-|n-m|/\ell(e))$

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CORRELATION FUNCTION $C(|n-m|) \sim \exp(-|n-m|/\ell(e))$



DRIVEN ATHERMAL DYNAMICS

$$m \ \ddot{x}_i = F_{\rm diss} + F_{\rm el} + F_{\rm ext}$$

Blocked configurations

$$\langle \xi_m \xi_n \rangle \sim G(|n-m|/\ell(e))$$

$$\ell(e) \sim e$$

$$e \sim \sqrt{?}$$

EFFECTIVE THERMODYNAMICS

$$\mathcal{Z} = \int_{\boldsymbol{\xi} \in \text{blocked}} \mathcal{D}\boldsymbol{\xi} \ e^{-\beta_{Ed} E[\boldsymbol{\xi}]}$$

$$\langle \xi_m \xi_n \rangle \sim C(|n-m|/\ell(e))$$

$$\ell(e) \sim e$$

$$e \sim \sqrt{T_{Ed}}$$

EDWARDS PARAMETER = DISSIPATED ENERGY





CONCLUSIONS

- We presented a 1D model where the effective thermodynamics " à la" Edwards works pretty well

- The model is simple and realistic: 1)"blocked" configurations are truly mechanically stable configurations; 2) Dry friction; 3) Dynamics is realistic

- The effective theory can be solved exactly by transfer operators

- The Edwards parameter ${\rm T}_{\rm Ed}\,$ has a clear physical interpretation: the energy dissipated in a driving cycle

PERSPECTIVES

- What happens in D=2?

- Diagonalization of (M^L x M^L) matrices: GPU
- M >> 1, discretization of continuous variable