

Flowing Matter Across the Scales, March 24th-27th 2015, Rome, Italy

Fluid dynamics of biologic and mechanical heart valves

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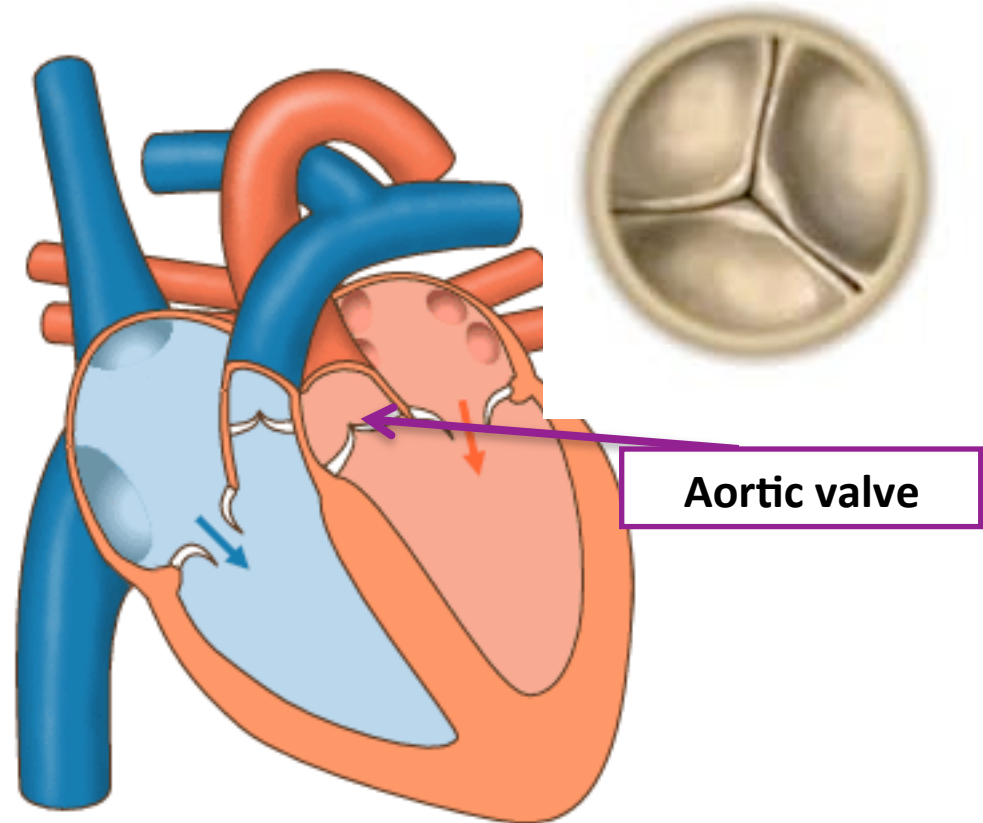
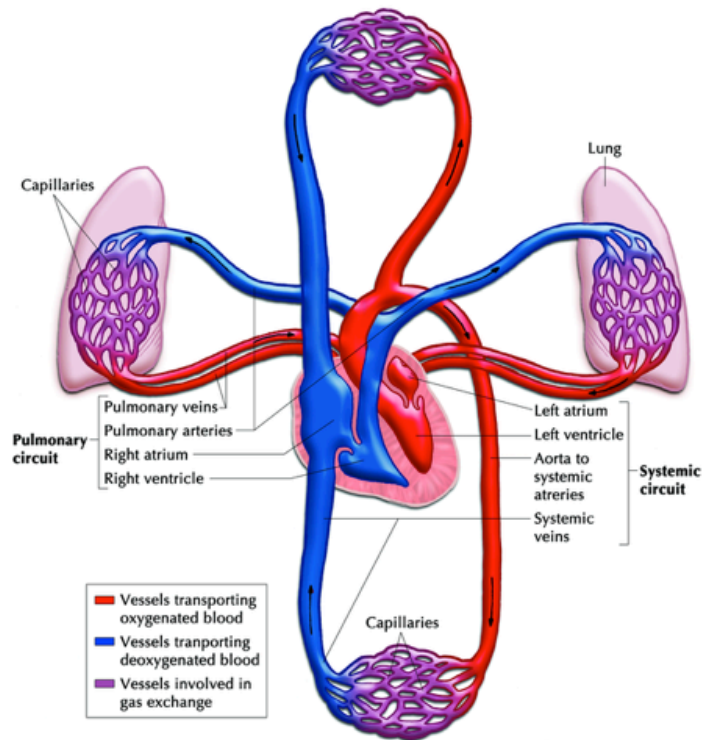
Thanks to:

L. Weltert, R. De Paulis *Cardiac Surgery Department, European Hospital, Rome, Italy*



BACKGROUND

The heart is made of two pumps (Left and Right) each composed of two chambers (ventricle and atrium) and valves that ensure the correct flow direction



The valves of the left side (Mitral and Aortic) are most commonly affected by diseases due to the large pressure they withstand (100-150 mmHg) and **sometimes they need replacement**

AORTIC VALVE REPLACEMENT (AVR)

Two main types of aortic valves are available:

Biologic



Mechanical



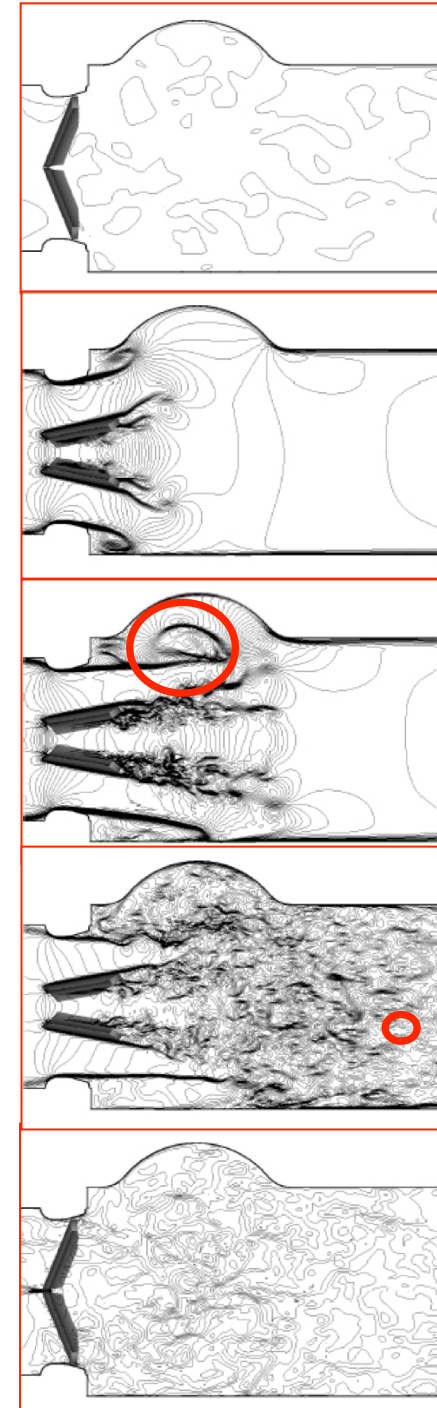
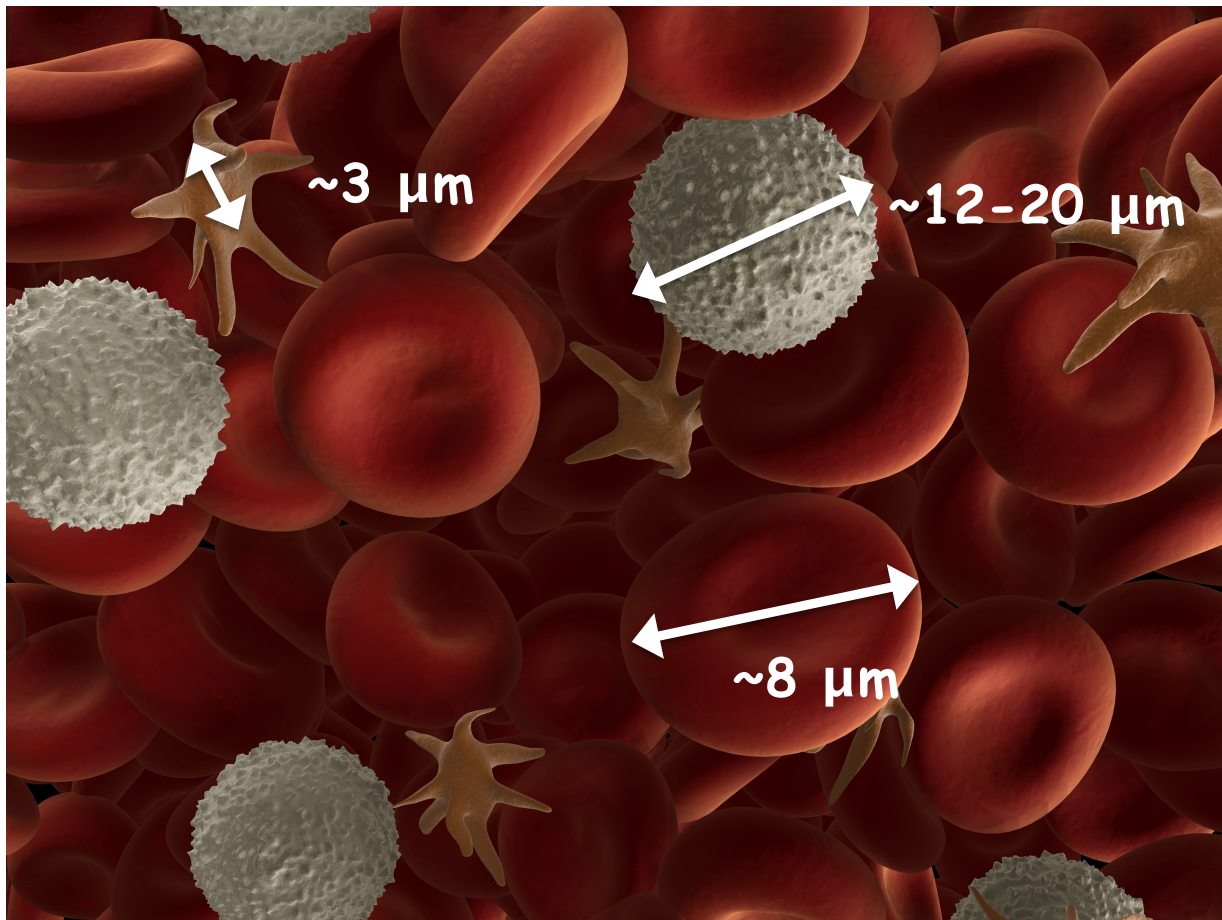
... each one having advantages and drawbacks

Biologic: 😊 good hemodynamic
☹️ limited durability (10-15 years)

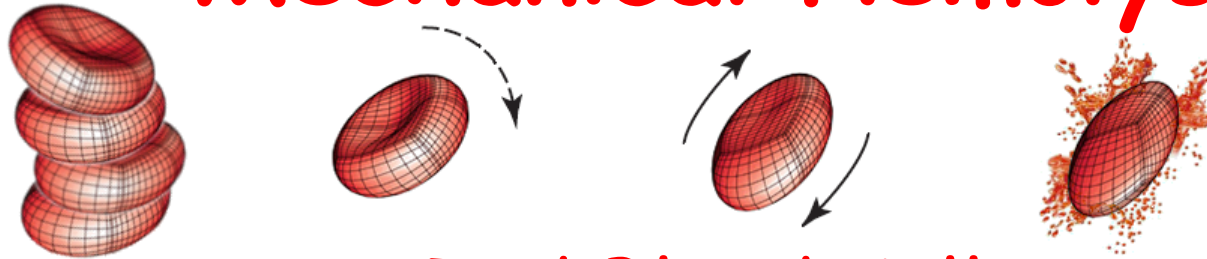
Mechanical: 😊 lifelong durability
☹️ *bad hemodynamics (need for anticoagulants)*
☹️ noise

WHY ANTICOAGULANTS FOR MHV?

The presence of obstacles in the flow enhances the energy cascade towards the smallest scales ($\sim 35\mu\text{m}$) that become comparable to the cells size



Mechanical Hemolysis



Shear

Red Blood Cell



The RBC's membrane stretches under the **shear stress**, develops pores and **hemoglobin is released into the plasma**.



The life span of RBCs drops from **122 ± 23** to **98.8 ± 23** days for **MHVs** (Mitlyng et al., American Journal of Cardiology 2006).

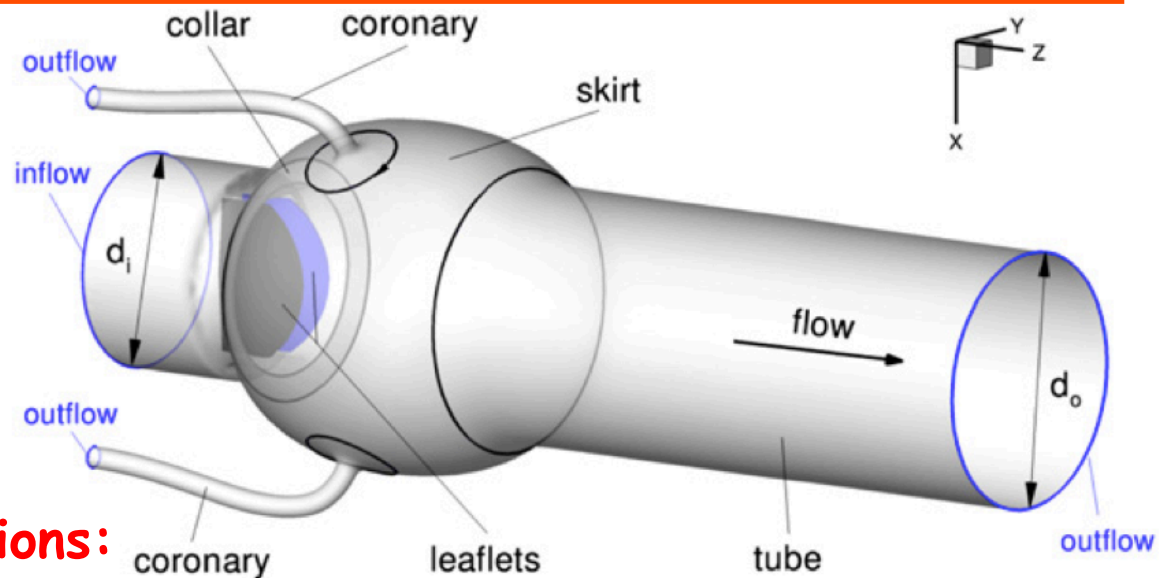
The altered stress levels activate platelets that stick to dead RBCs to form **clots**



Numerical study of the problem

- Immersed Boundary Technique
- Direct Numerical Simulation fluid solver
- Structural solver
- Fluid-Structure-Interaction

2nd order accurate
(in space and time)



Typical physiological conditions:

Cycle period: 866 ms (70 bpm)

Mean flowrate: 5 l/min

Peak flowrate: 28 l/min

$Re_{peak} = 6200$

$\approx 20M$ nodes

$dt = 2-200 \mu s$

STRONG COUPLING (FLUID/VALVE)

$$\frac{D\mathbf{u}}{Dt} = -\frac{\nabla p}{\rho} + \frac{1}{\rho} \nabla \cdot \boldsymbol{\tau} + \mathbf{f}$$

$$\nabla \cdot \mathbf{u} = 0$$

$$M \frac{d^2 \mathbf{x}}{dt^2} = \mathbf{F} \quad \mathbf{F} = \int_s (\boldsymbol{\tau} \cdot \mathbf{n} - pn) dS$$

$$\mathbf{I} \frac{d^2 \boldsymbol{\theta}}{dt^2} = \mathbf{T} \quad \mathbf{T} = \int_s [\mathbf{r} \times (\boldsymbol{\tau} \cdot \mathbf{n} - pn)] dS$$



(de Tullio et al, 2009)

(Borazjani et al, 2008)

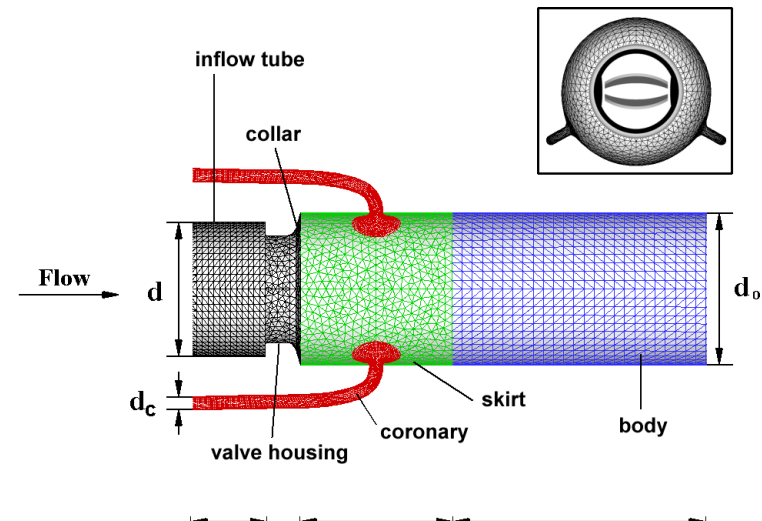
WEAK COUPLING (FLUID/AORTIC WALL)

$$\frac{D\mathbf{u}}{Dt} = -\frac{\nabla p}{\rho} + \frac{1}{\rho} \nabla \cdot \boldsymbol{\tau} + \mathbf{f}$$

$$\nabla \cdot \mathbf{u} = 0$$

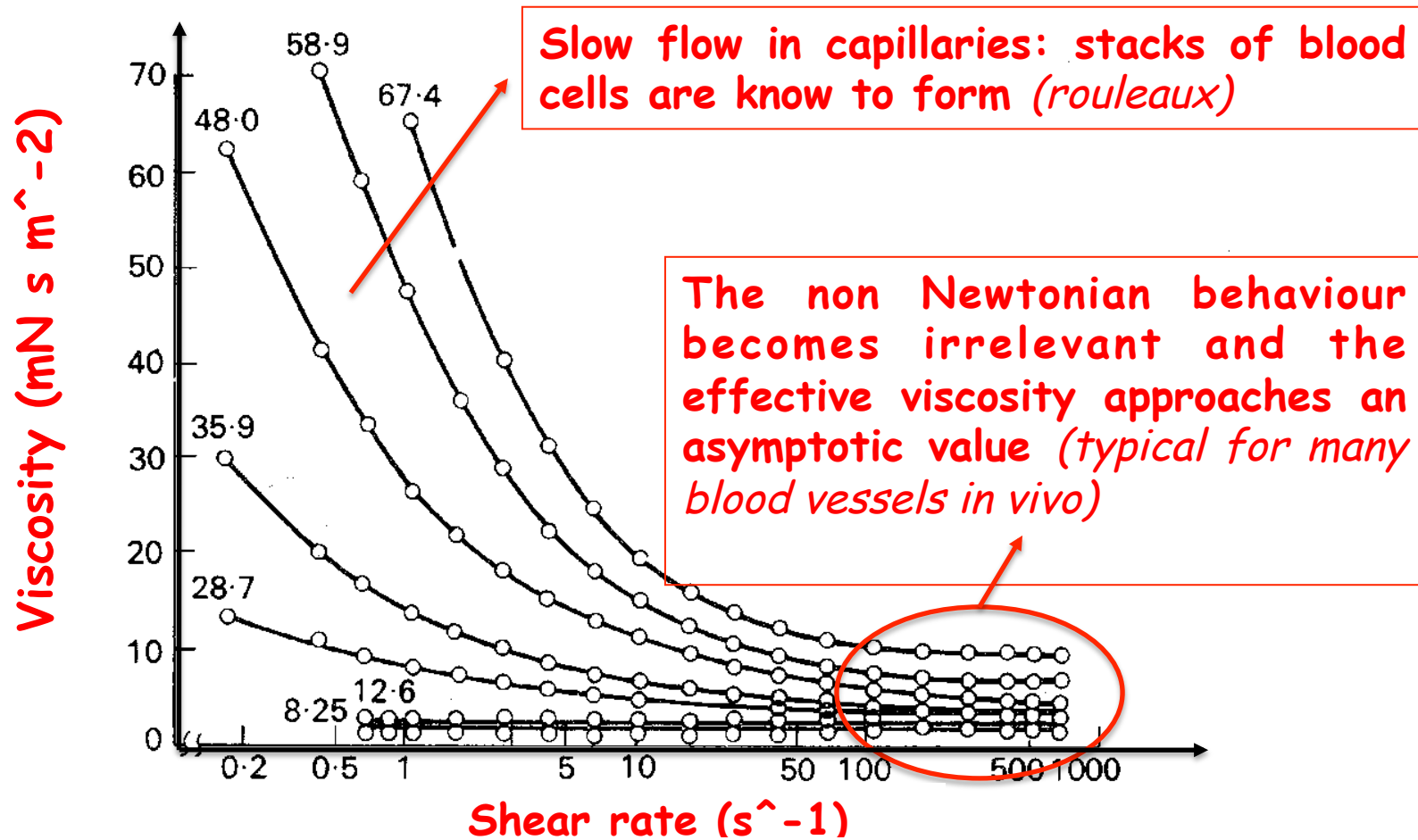
$$\nabla \cdot \boldsymbol{\sigma}_s = \rho_s \frac{\partial^2 d_s}{\partial t^2} \quad \boldsymbol{\sigma}_s = C E_s$$

$$E_s = \frac{1}{2} [\nabla \cdot d_s + (\nabla \cdot d_s)^T + (\nabla \cdot d_s)^T \nabla \cdot d_s]$$



BLOOD AS A NEWTONIAN FLUID

Blood: flexible red cells suspended in a Newtonian flow, the plasma



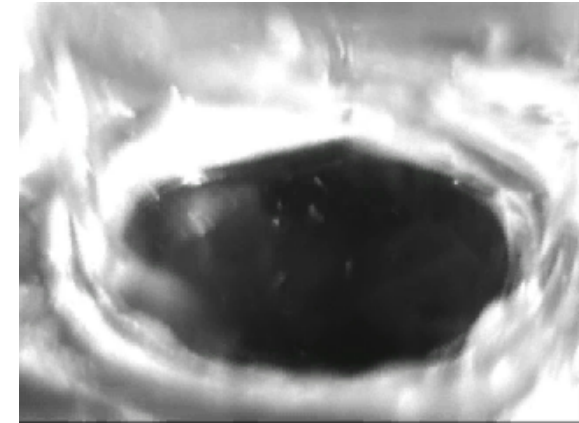
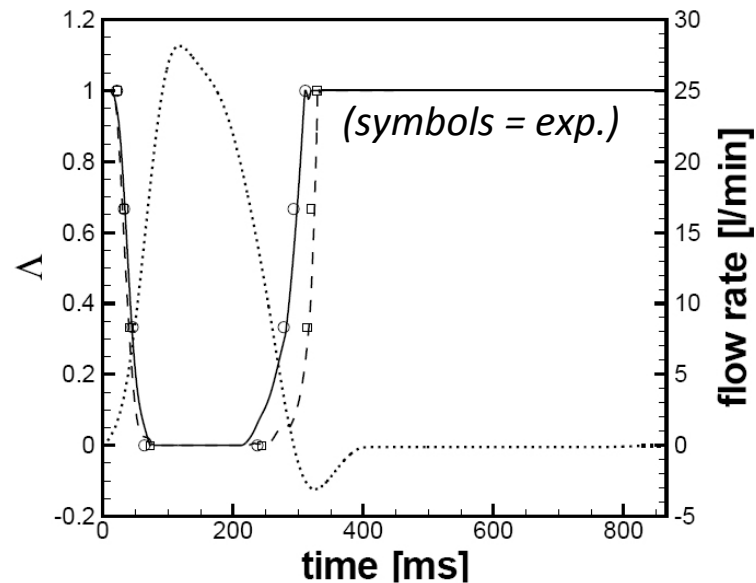
Shear rate/viscosity relationship for human blood 25°C for various hematocrit values (Brooks et al, 1970, *J. appl. Physiol.* 28)

To be further discussed

Validation with in-vitro experiments

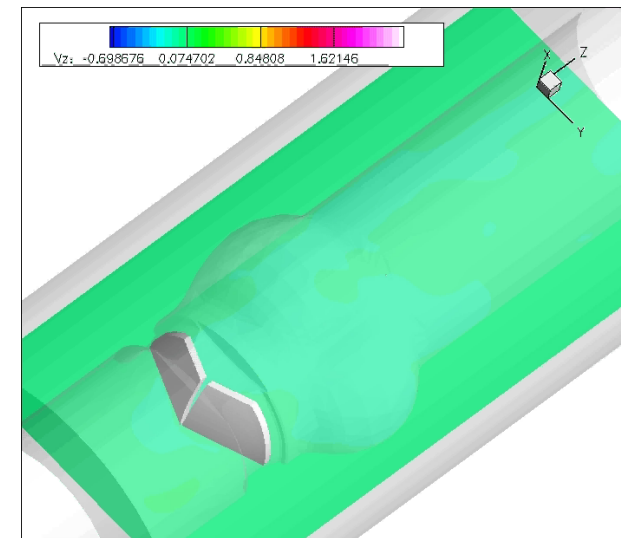
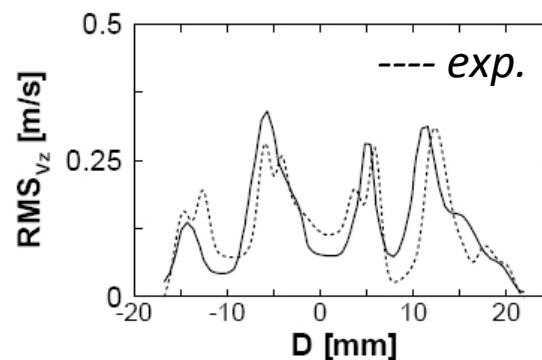
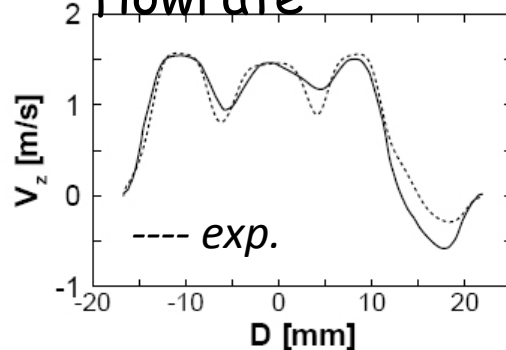
(RIGID LEAFLETS)

- Phase-averaged leaflets angular position



Experiments by
G-P-Romano & G. Querzoli

- Phase-averaged profiles at peak of flowrate

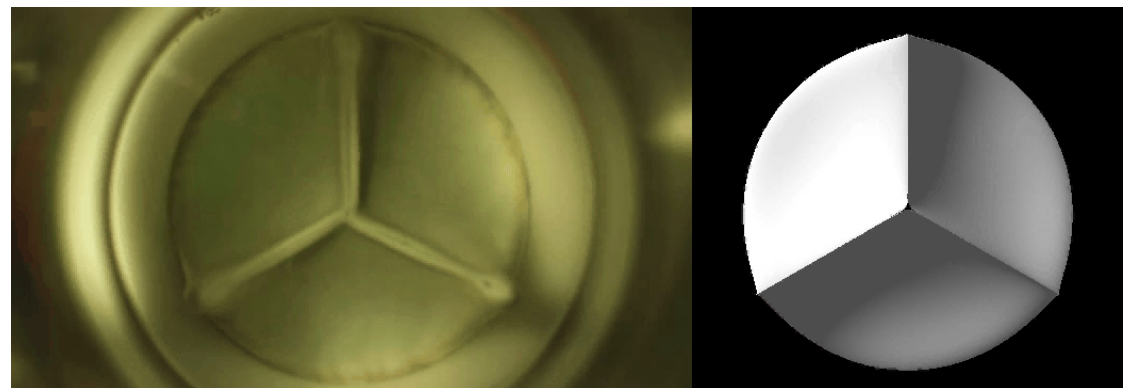
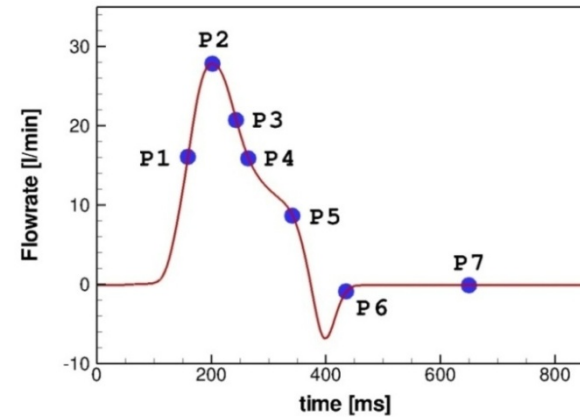
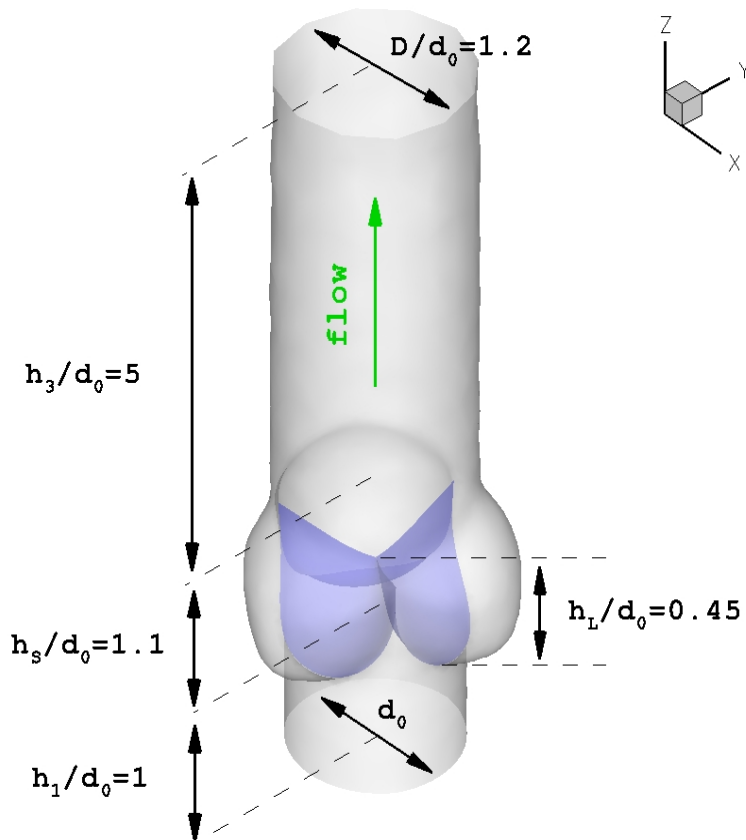


(de Tullio et al., JFM, 2009)

Validation with in-vitro experiments

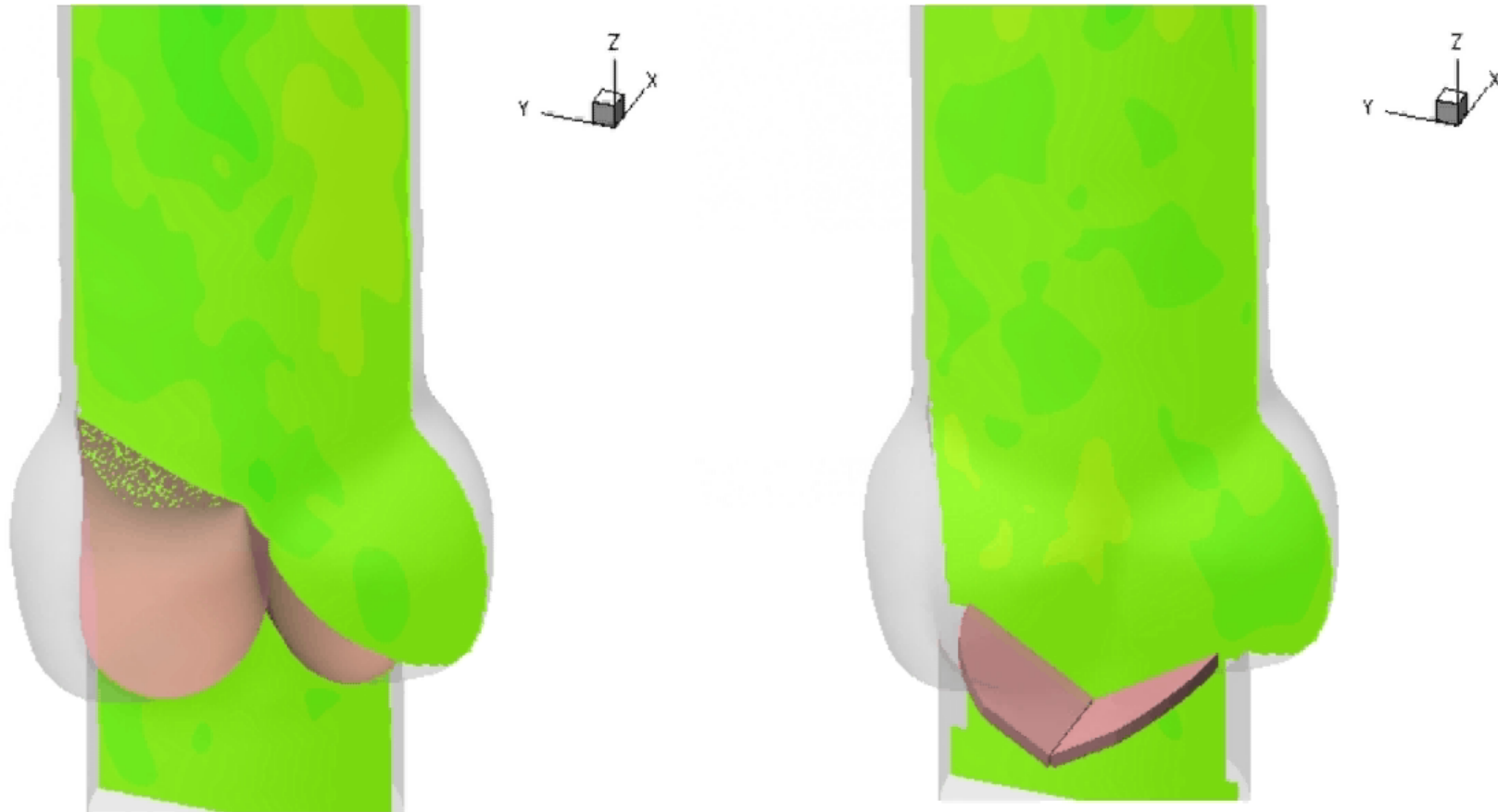
(DEFORMABLE LEAFLETS)

- Cardiac output: 5 l/min;
- Beat rate: 70 beats/min;
- Peak Reynolds number: 6200;



Experiments from St. Jude Medical Inc. (www.sjm.com)

Biologic vs Mechanical

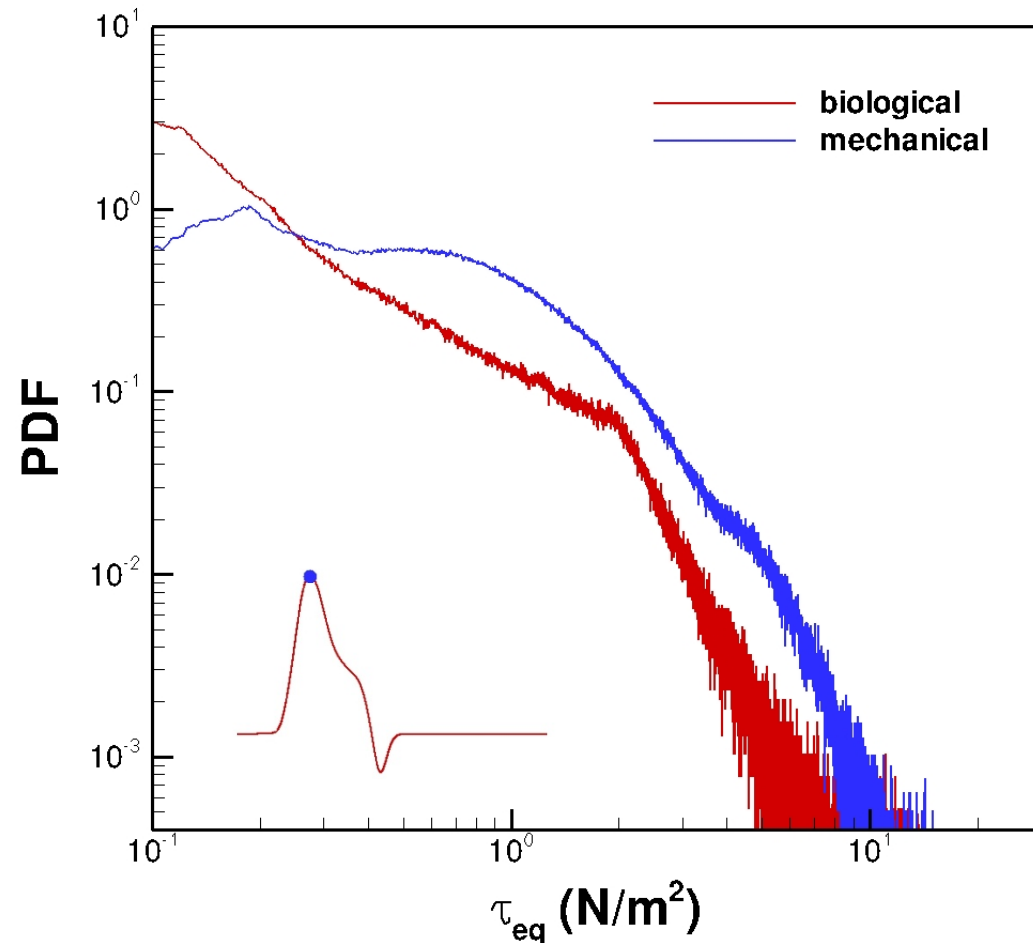
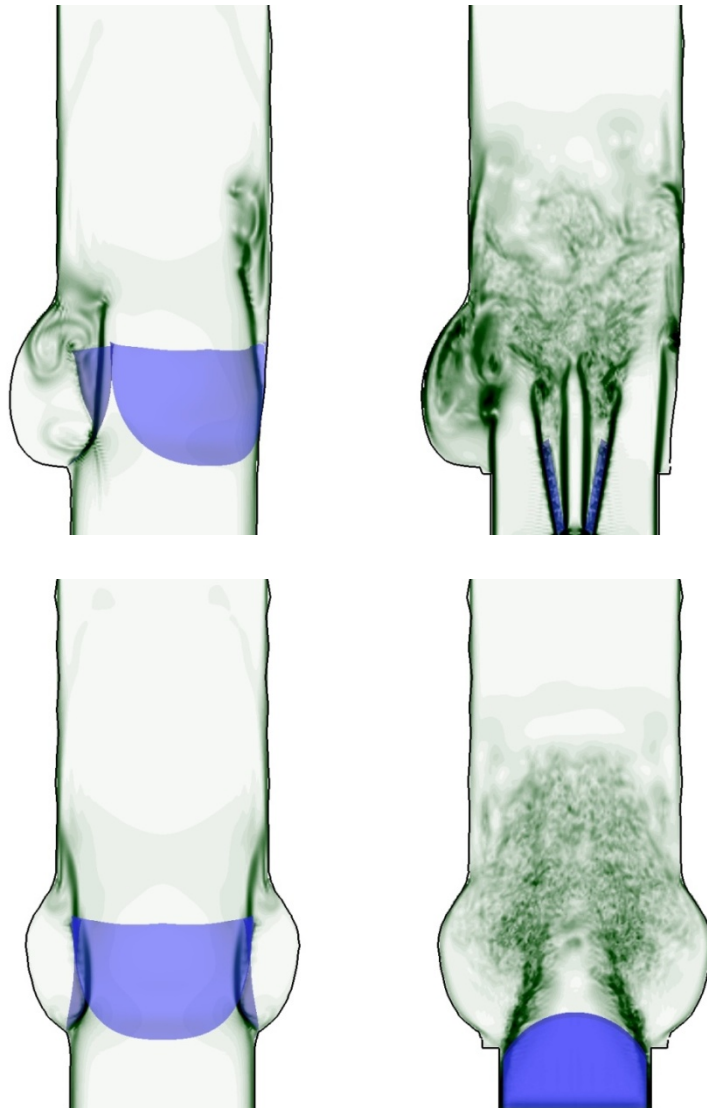


Contours of streamwise velocity in the YZ plane

Comparison of Eulerian viscous stresses

Equivalent viscous stress

$$\tau_{eq} = (3\tau_{ij}\tau_{ij}/2)^{1/2}$$



Eulerian quantities are not enough because they do not account for the exposure time to a given stress level

Hemolysis computation

Hemolysis is the result of the damage *history* (stress level and exposure time) of RBC therefore it has to be evaluated along their trajectories

Small volumes of blood still considered as a single fluid:

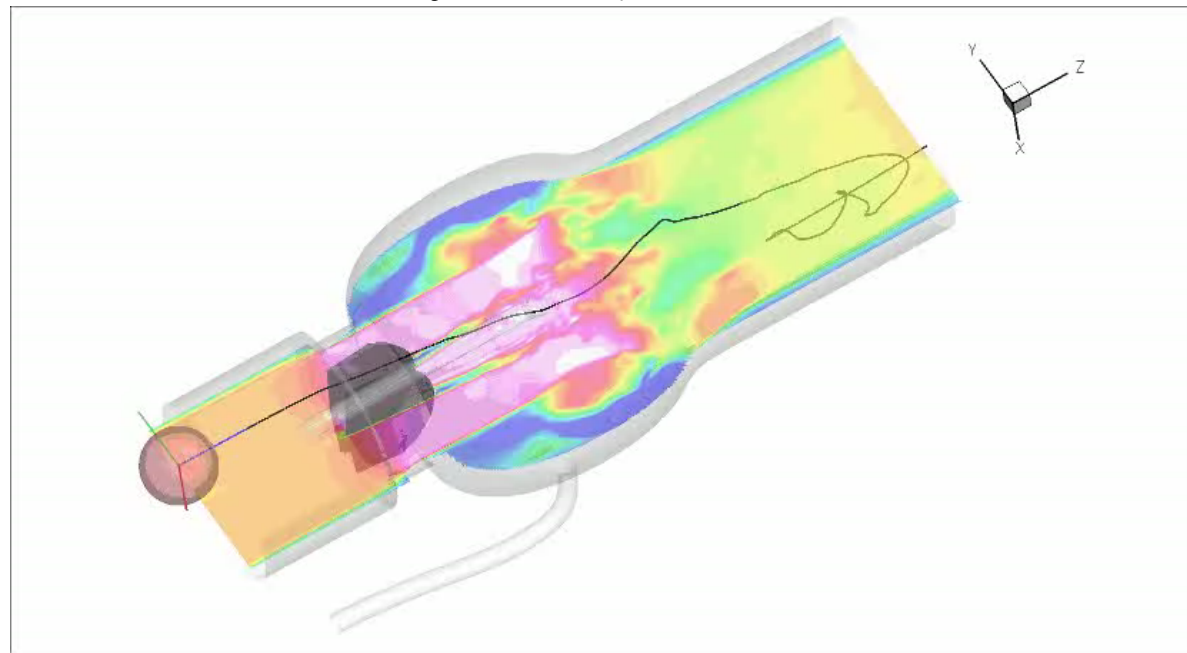
Lagrangian tracers

$$\dot{\mathbf{x}}(t) = \mathbf{u}$$

The damage model is integrated over each cell's trajectory



$4 \cdot 10^5$ tracers per-cycle injected



Deformation of a single fluid particle

MORFOLOGY TENSOR EVOLUTION

$$\frac{d\mathbf{S}}{dt} = (1 - f_2) [\boldsymbol{\Omega} \cdot \mathbf{S} - \mathbf{S} \cdot \boldsymbol{\Omega}] \quad \text{Maffettone et al. (1998)}$$

$$= -f_1 [\mathbf{S} - g(\mathbf{S})\mathbf{I}] + f_2 [\nabla \mathbf{u} \cdot \mathbf{S} + \mathbf{S} \cdot \nabla \mathbf{u}^T]$$

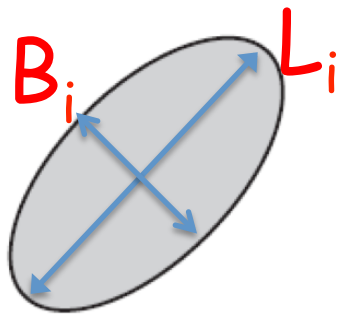
$$g(\mathbf{S}) = 3 \cdot III / II \quad \nabla \mathbf{u} \text{ velocity gradient tensor}$$

$$\boldsymbol{\Omega} \text{ rotation rate tensor}$$

$$f_1 = 5.0 \text{ s}^{-1} \quad \text{Specific parameters for red- Arora et al. (2004)}$$

$$f_2 = 4.2298 \cdot 10^{-4} \quad \text{blood cells of human blood}$$

At every i -th time step the \mathbf{S} morfology tensor is evolved along the Lagrangian trajectory. The \mathbf{S} eigenvalues are the axes of the ellipsoidal cell



$$\phi_i = \frac{L_i - B_i}{L_i + B_i}$$

shape factor

$$\tau = \mu \frac{2\phi_i f_1}{(1 - \phi_i^2) f_2}$$

fluid particle stress

BLOOD DAMAGE

Tracking deformable particles (*no back-reaction on the fluid*) and interpolating along the trajectory all the needed quantities (blood is considered as a single fluid)

$$\dot{\mathbf{x}}(t) = \mathbf{u}$$

viscous stress tensor has been reduced to a single scalar quantity according to the morphology tensor equation (*Arora, 2004*)

$$\tau = \mu \frac{2\phi_i f_1}{(1 - \phi_i^2) f_2}$$

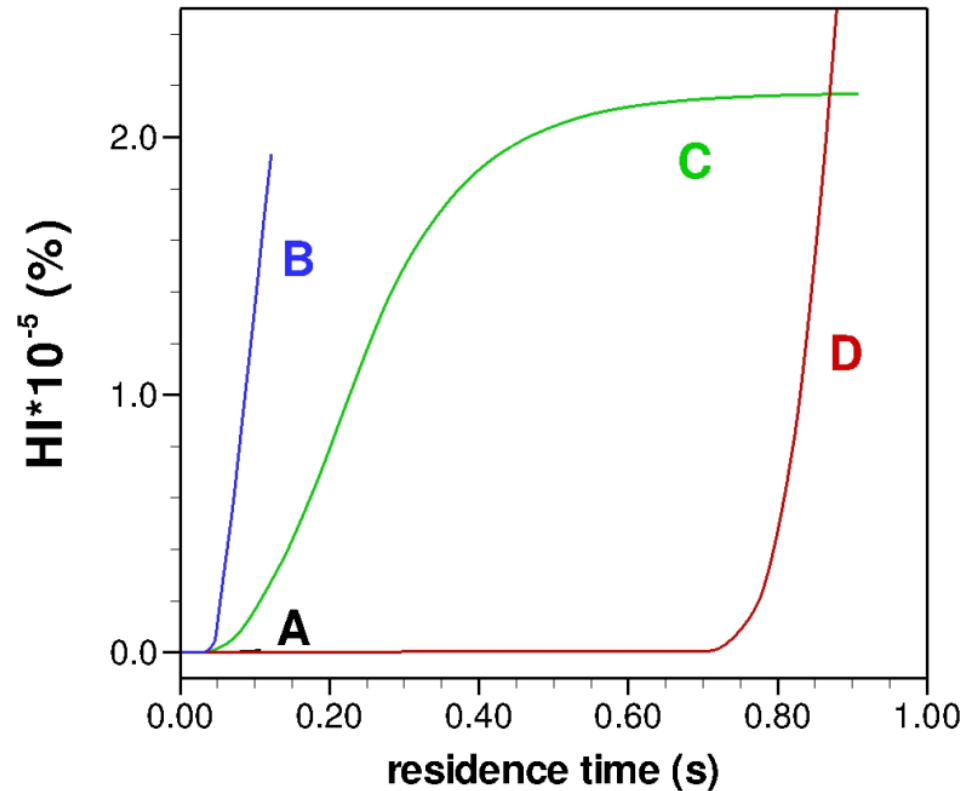
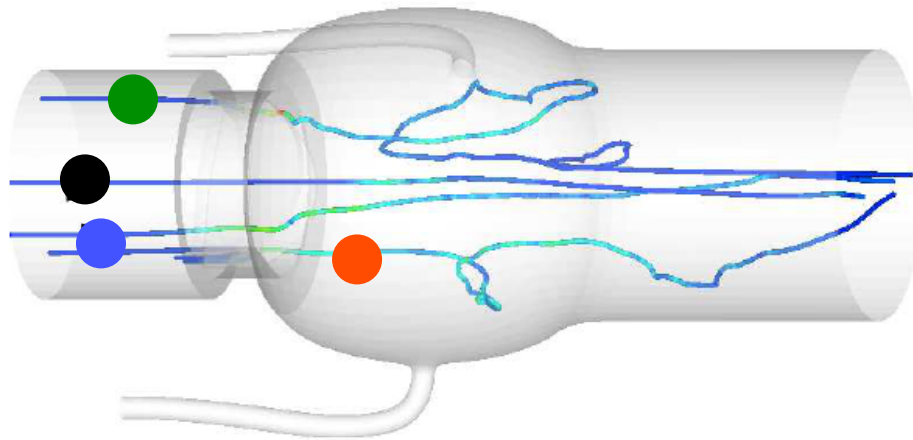
With the information on stresses and exposure times, it is possible to compute the Hemolysis Index (*Goubergrits, 2006*):

$$\Delta HI_i = \alpha C t_i^{\alpha-1} \tau(t_i)^\beta \Delta t_i$$

$C=3.62 \times 10^{-5}$, $\beta=2.416$, $\alpha=0.785$ for RBC

$C=1 \times 10^{-5}$, $\beta=0.625$, $\alpha=1.320$ for platelets

Hemolysis Index



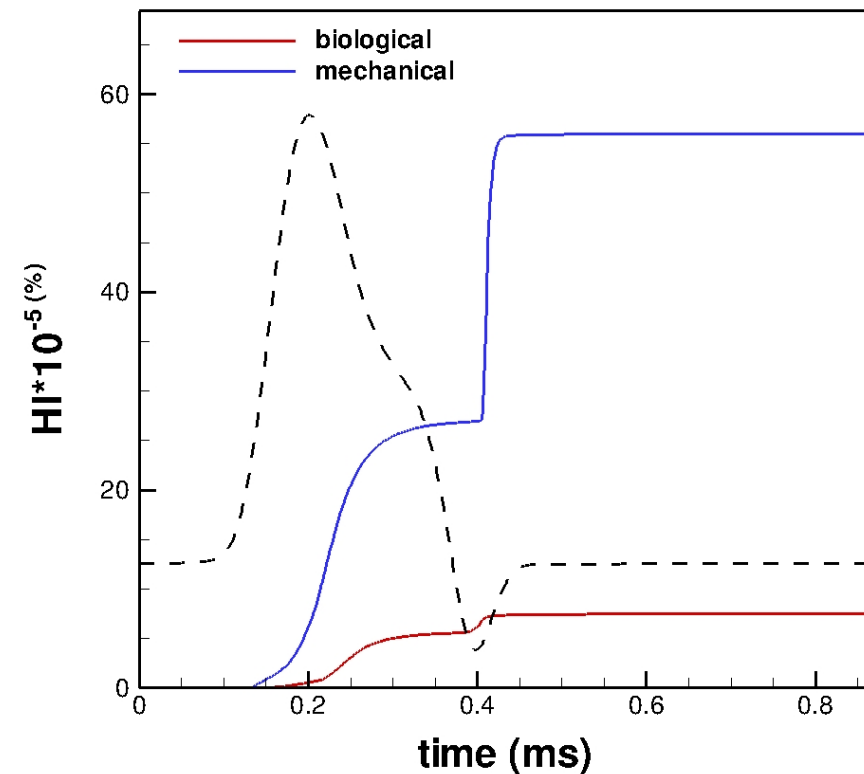
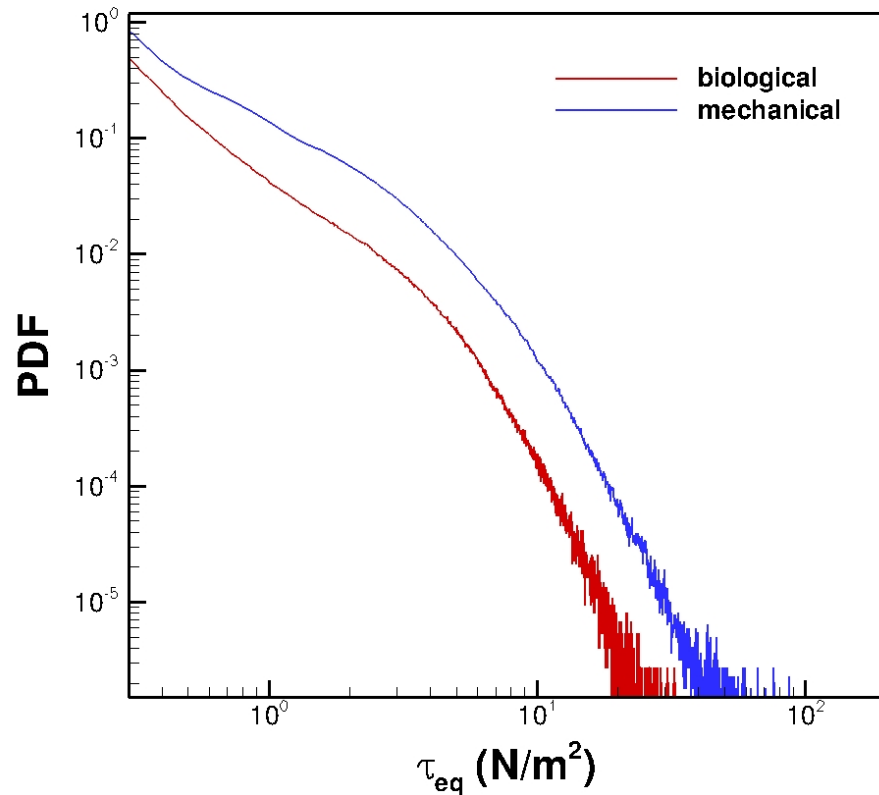
Will this occur to every red cell?

- The mean flow rate is **5 l/min**, the total volume of blood about **5 l** and the half-life-time of red cells about **120 days**, therefore each red cell will cross the valve **173000** times! This implies that even an unlikely event (like the crossing of the hinge) will occur several times to each cell.

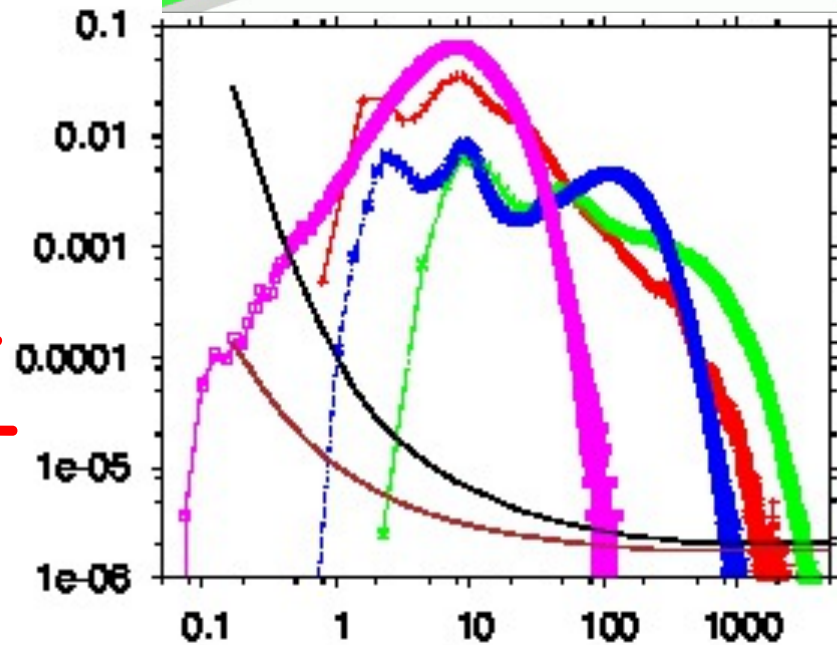
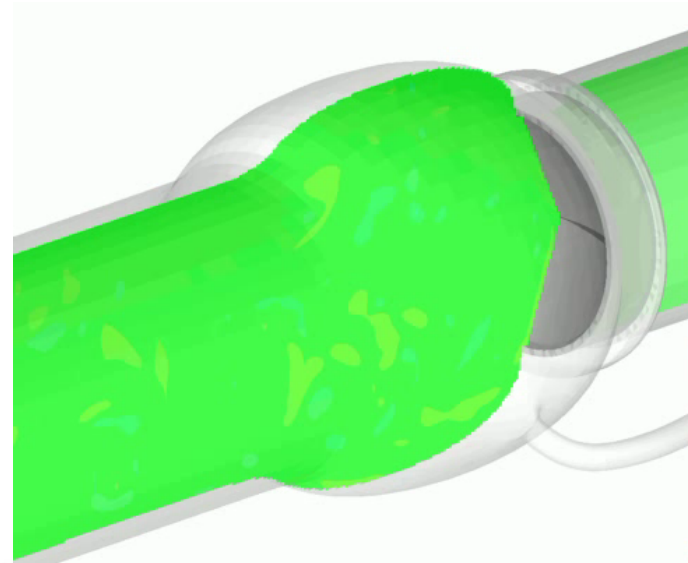
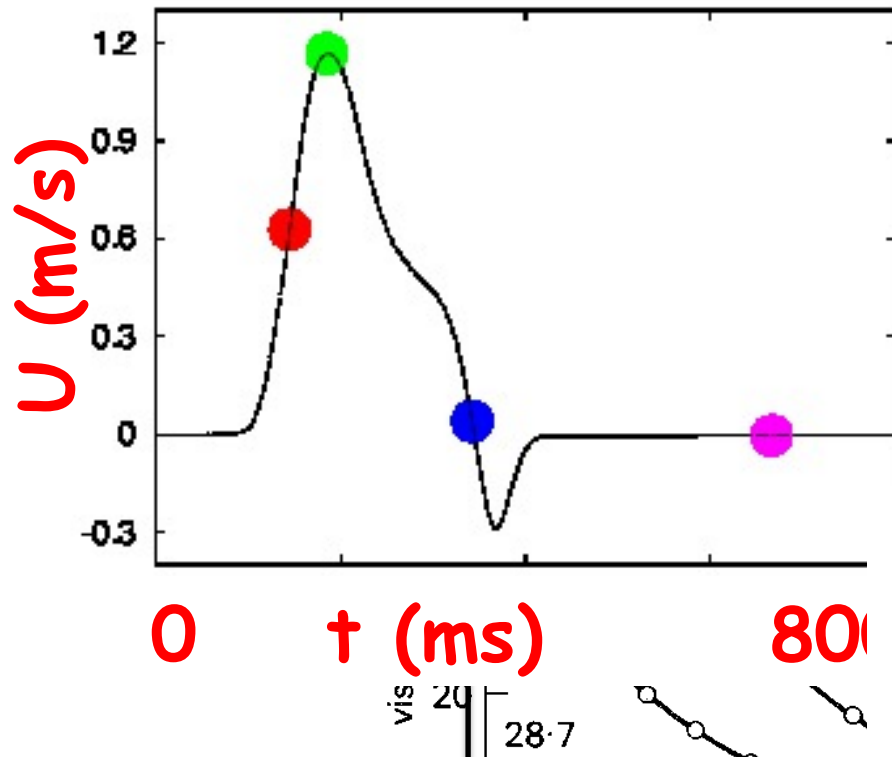
Lagrangian hemolysis results

Particles crossing the devices only once:

	mean τ_{eq} (N/m ²)	mean residence time (s)	mean HI (%)
Biological	0.236	0.37	$3.87 \cdot 10^{-5}$ %
Mechanical	0.677	0.42	$3.71 \cdot 10^{-4}$ %



IS BLOOD IN LARGE ARTERIES REALLY A NEWTONIAN FLUID?



The non-Newtonian fluid nature might be relevant

(Brooks et al, 1970, J. appl. Physi

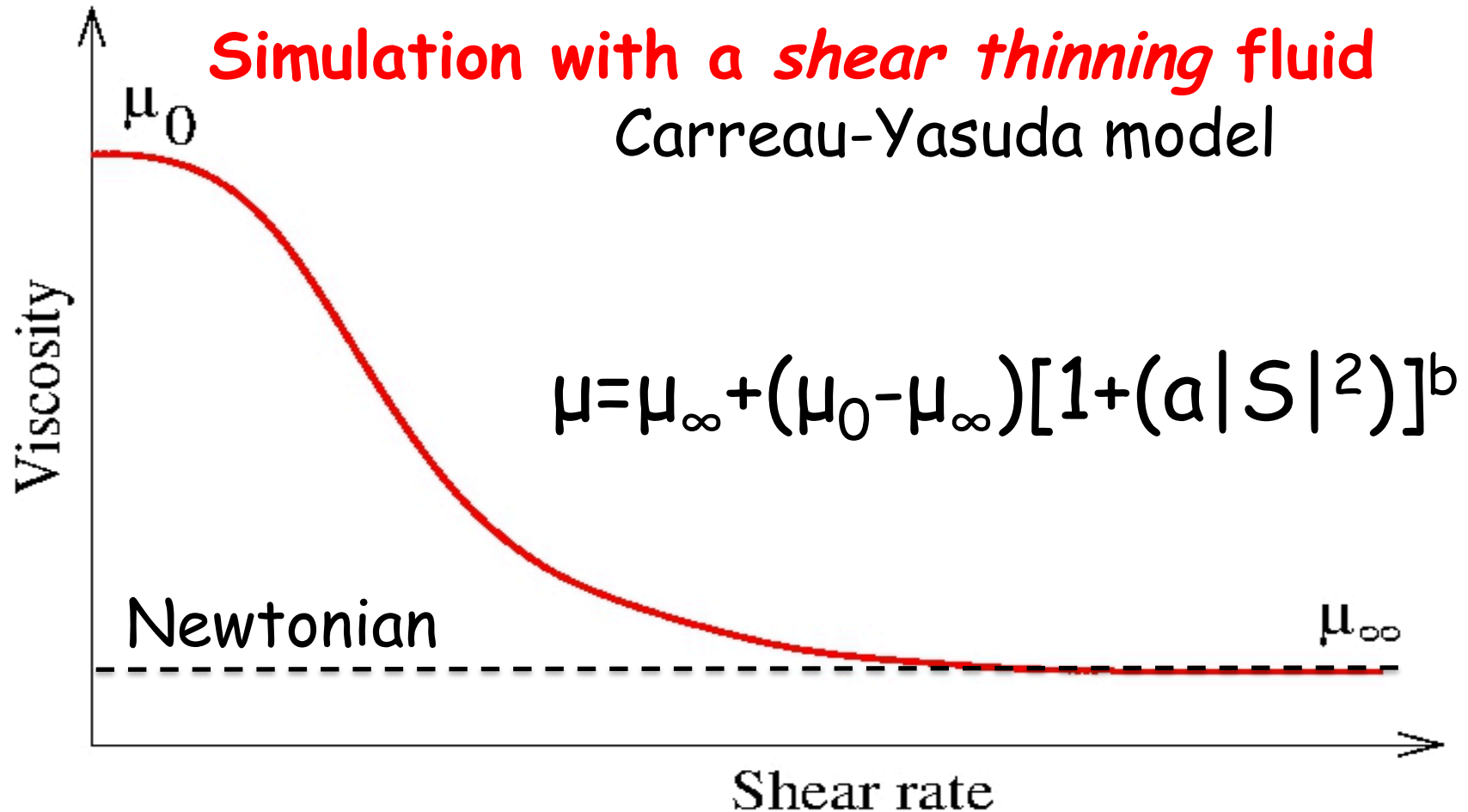
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Viscosity (mN s m⁻²)

Shear rate (s⁻¹)

Simulation with a *shear thinning* fluid

Carreau-Yasuda model



a , b , μ_0 and μ_∞ are hematocrit dependent parameters

$\mu_\infty = 3.5 \times 10^{-6}$ Pa s, $\mu_0 = 5.6 \times 10^{-5}$ Pa s

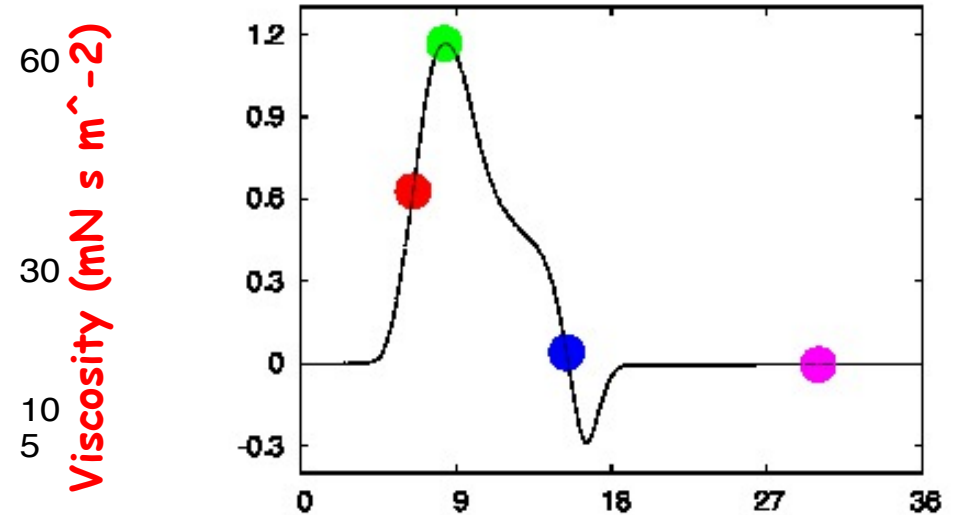
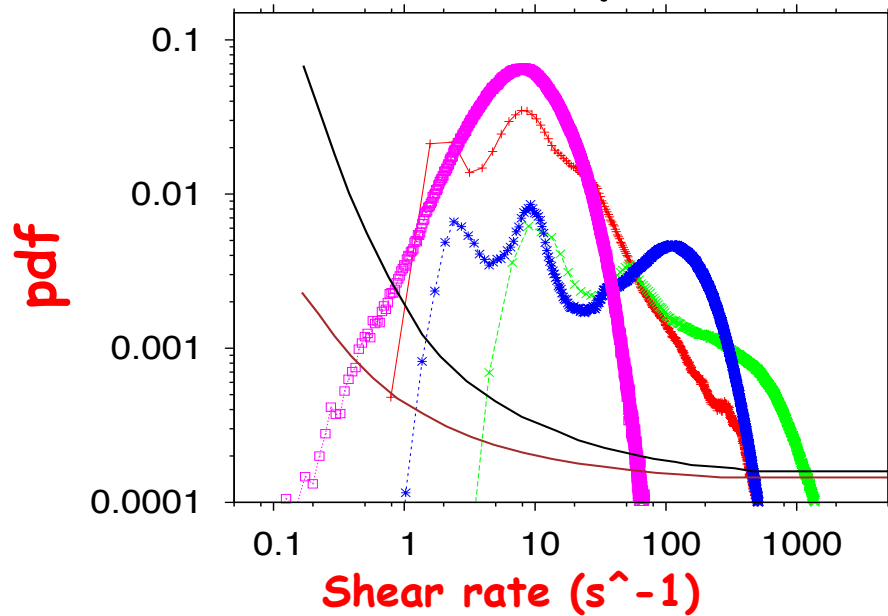
$a = 3.313$ s, $b = -0.3216$

for a man with ~40% of hematocrit

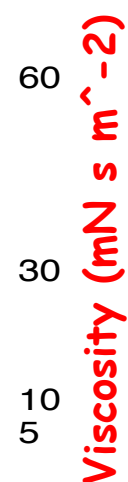
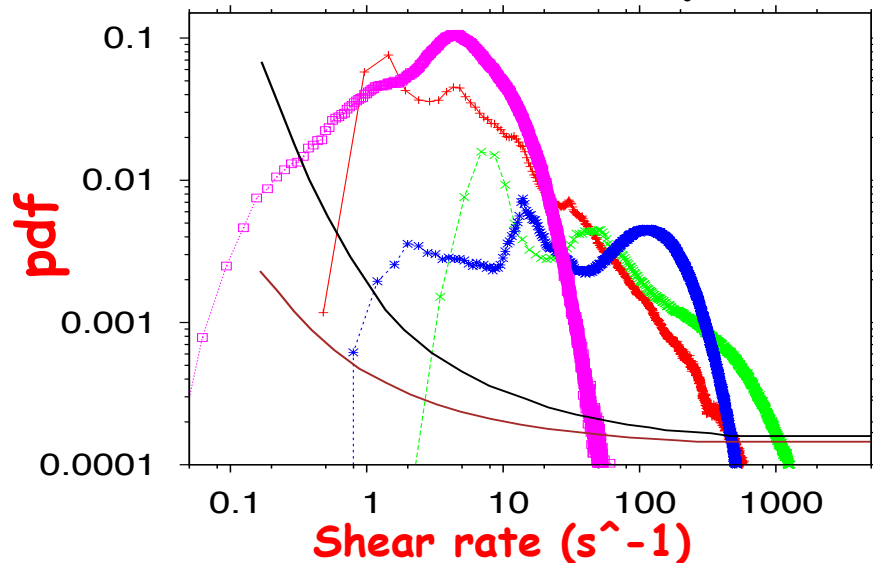
Note: only the shear-thinning behaviour is accounted for and not the viscoelastic (time-dependent) features.

Comparison between shear-rate pdfs'

Newtonian fluid



non-Newtonian fluid



There are differences both at low and high shear-rates.

The red-blood cells damage (hemolysis) is likely to be different.

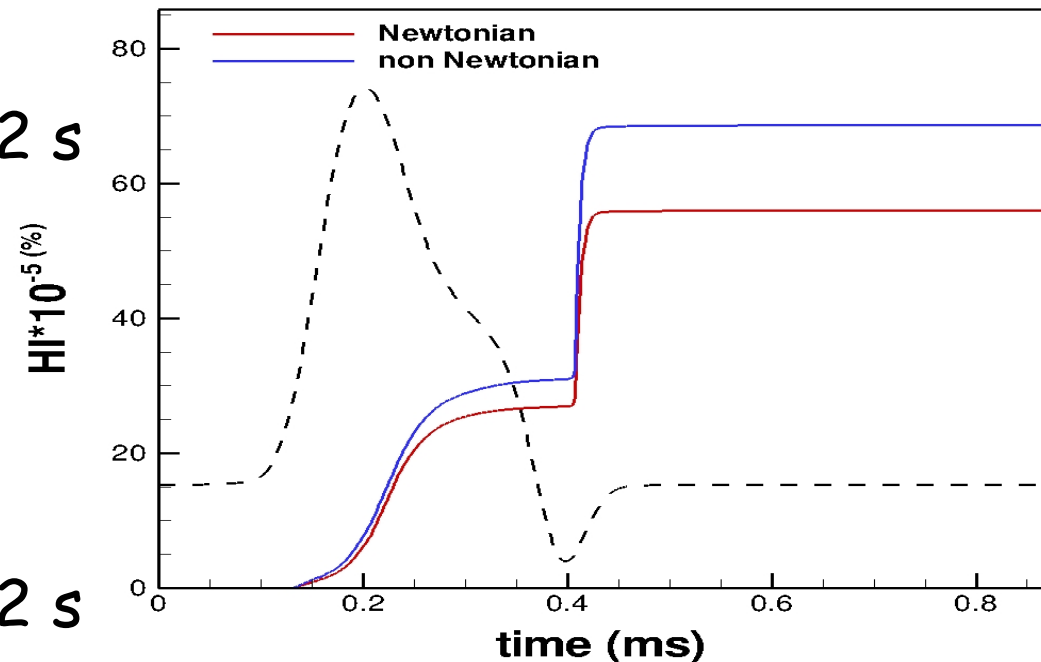
Comparison between hemolyses

Newtonian fluid

- mean $\tau_{eq} = 0.677 \text{ N/m}^2$
- mean HI = $3.71 \cdot 10^{-4} \%$
- mean residence time: 0.42 s

non-Newtonian fluid

- mean $\tau_{eq} = 0.769 \text{ N/m}^2$
- mean HI = $4.31 \cdot 10^{-4} \%$
- mean residence time: 0.42 s



The (averaged) hemolysis is larger for the non-Newtonian fluid ($\approx 14\%$).

Closing Remarks

A cost/efficient numerical method for biomedical applications is a valid tool complementary to in vitro and in vivo experiments

Biological valves have better hemodynamics than mechanical valves because they reduce the viscous stress levels in the blood and the exposure time.

The "price of success" is that biological valves have not a lifelong duration and they need to be replaced after ~15 years

The non-Newtonian nature of the blood has some effect on the hemolysis

Ongoing work: **modelling the complete heart**

Multidisciplinary collaboration project between medicine and engineering



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Univ. of Twente NL

