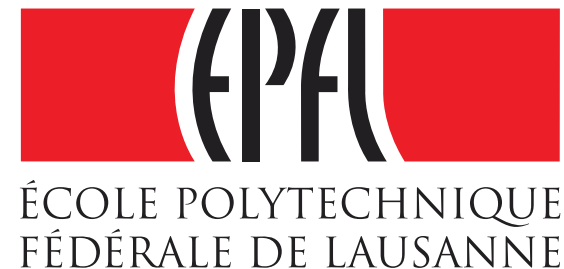


A depth-averaged model for droplets in thin microfluidic channels

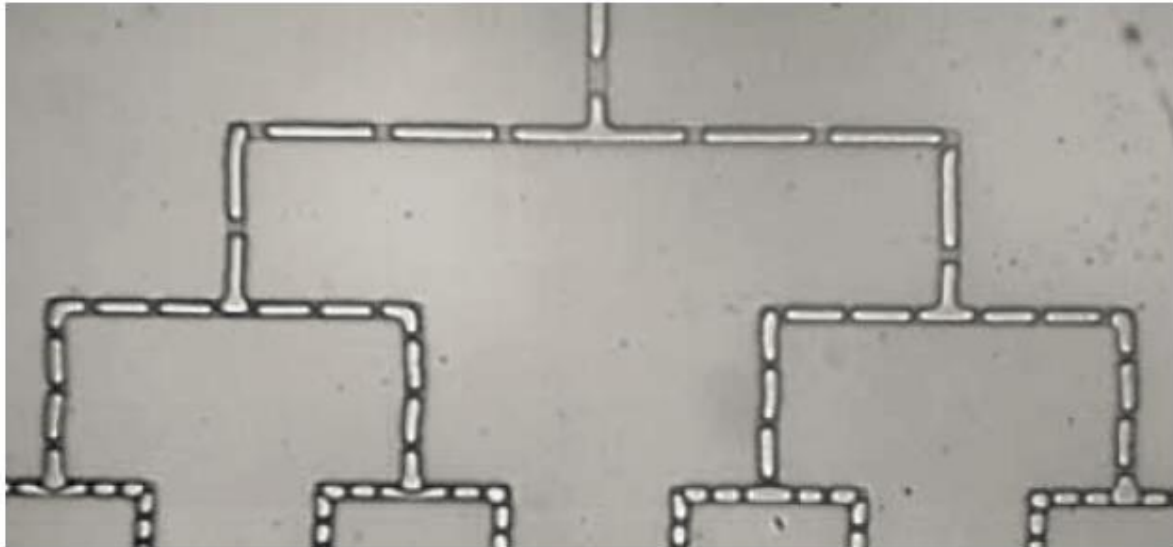
Mathias Nagel, P.-T. Brun and François Gallaire

LFMI

EPFL, Lausanne, Switzerland

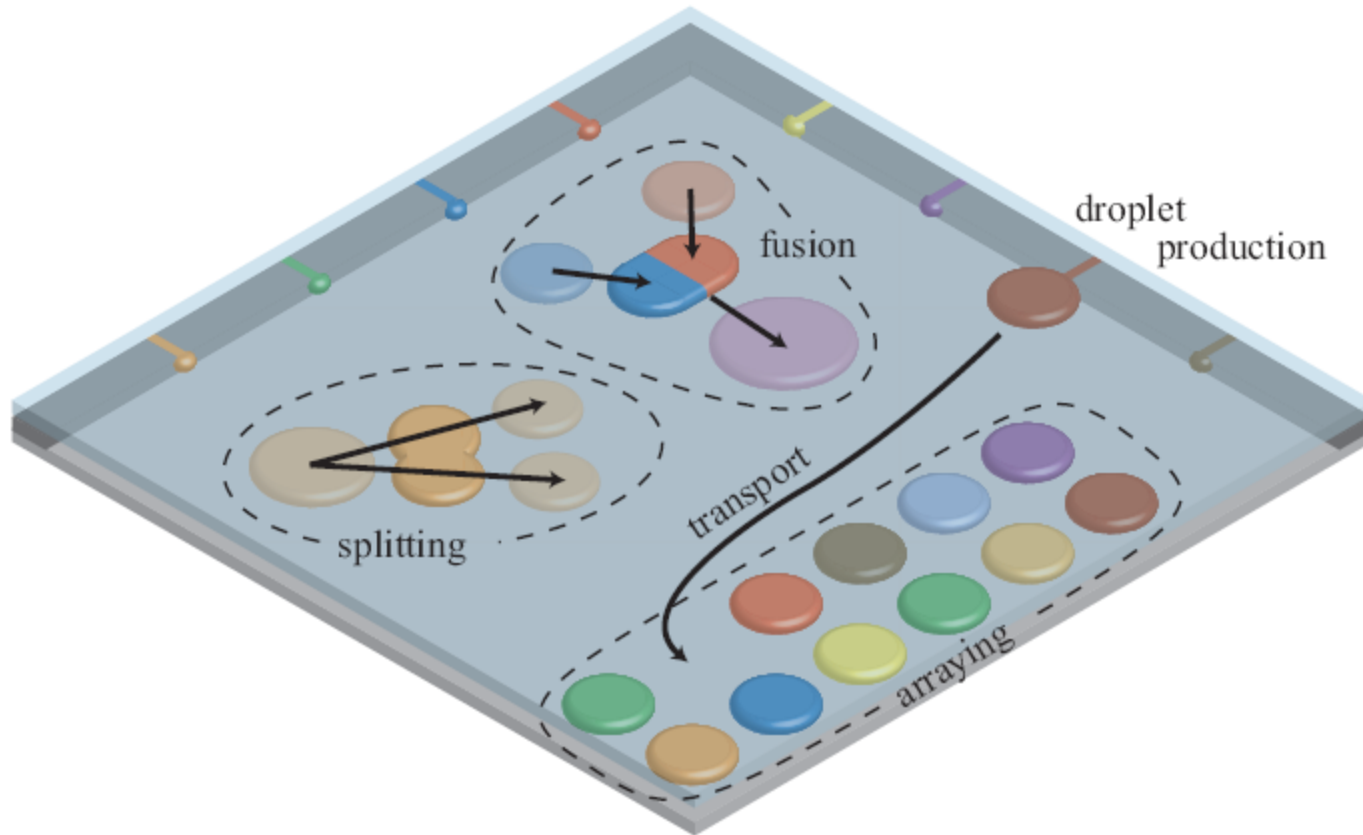


Droplet microfluidics



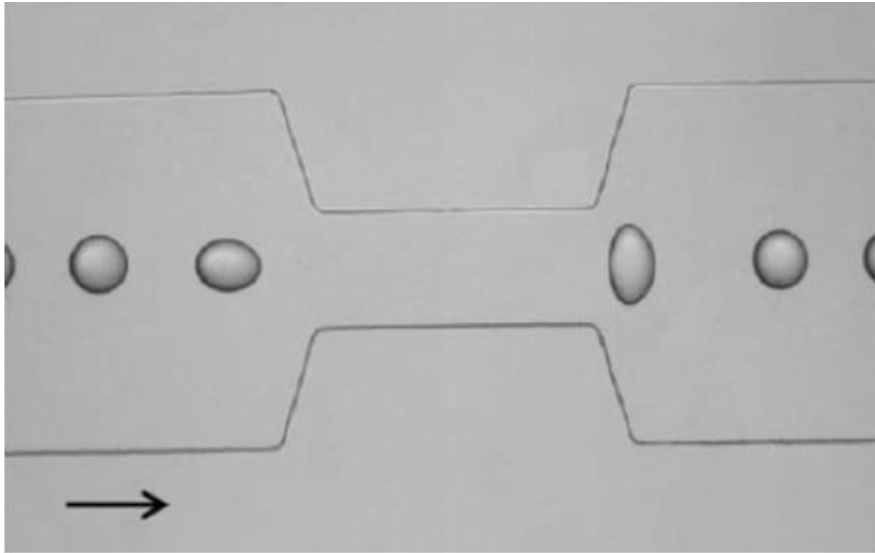
Link *et al.*, Phys. Rev. Lett. (2004)

2D Droplet microfluidics

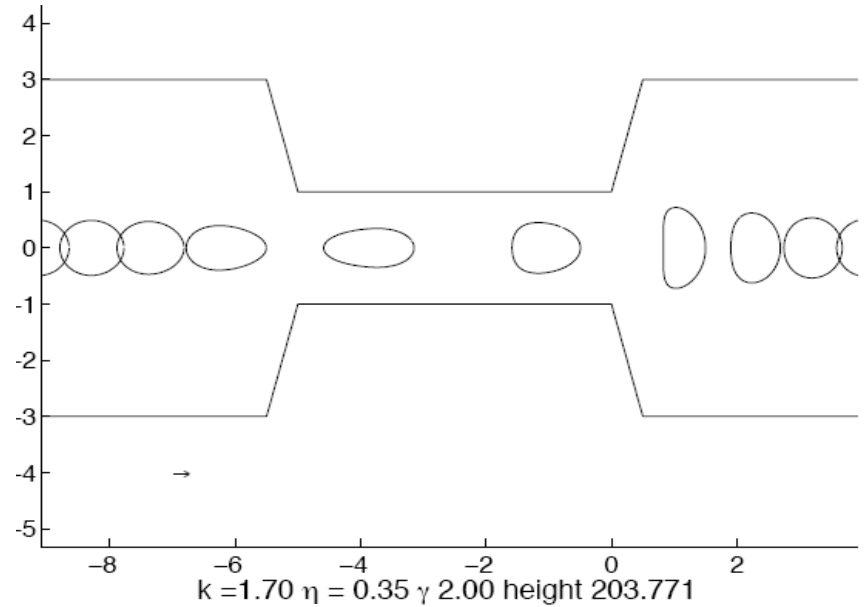


Dangla et al. (2012)

Need for accurate simulations of moving droplets in thin microchannels

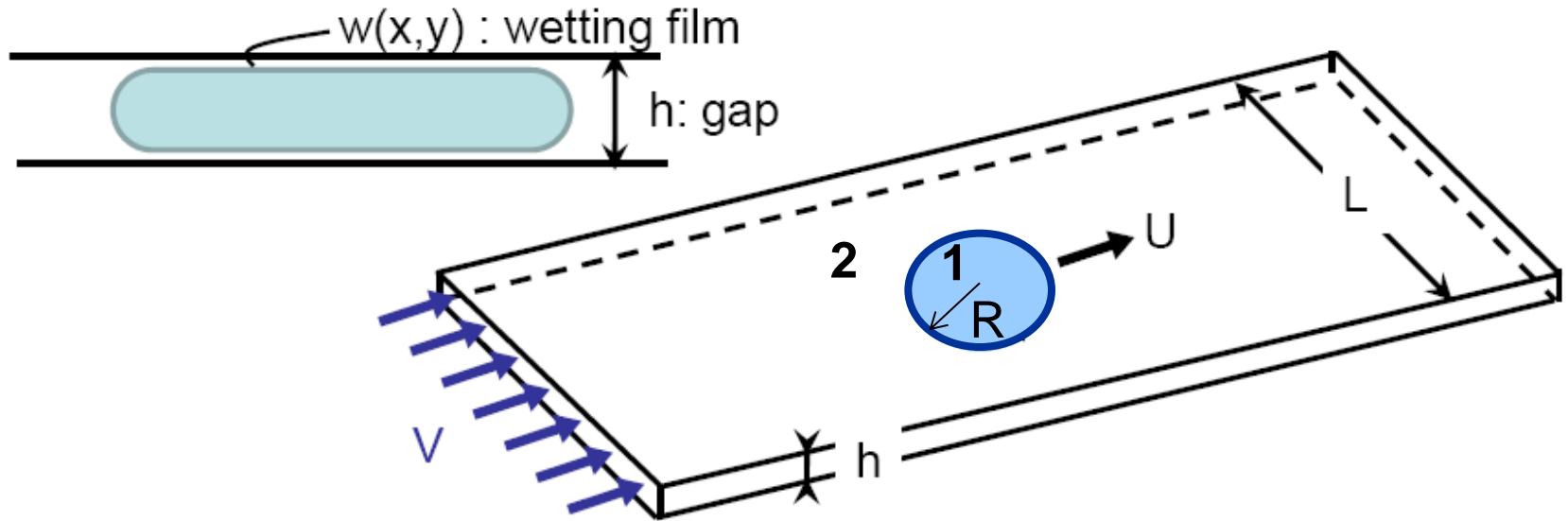


Experimental (by Cabral and Hudson)



Numerical

Thin microchannels look like Hele-Shaw cells



- Stokes flow (low Re)
- Thin channel $h/R \ll 1$
- Unbounded outer flow ($L/R \gg 1$)

• Capillary number

$$Ca = \frac{\mu U}{\gamma}$$

Hele Shaw flows : Darcy approximation

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

$$\mu \frac{\partial^2 u}{\partial z^2} = \frac{\partial p}{\partial x}$$

$$\mu \frac{\partial^2 v}{\partial z^2} = \frac{\partial p}{\partial y}$$

$$\frac{\partial p}{\partial z} = 0$$

$$\varepsilon \ll 1$$

$$\text{Re } \varepsilon \ll 1$$

Hele Shaw flows : Darcy approximation

$$u(x, y, z) = -\frac{1}{2\mu} \frac{\partial p}{\partial x} z(h-z)$$

$$v(x, y, z) = -\frac{1}{2\mu} \frac{\partial p}{\partial y} z(h-z)$$

$$w(x, y, z) = 0 !$$

$$\omega_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 0 !$$

Potential flow
in the (x-y) plane

$$\nabla p = -k^2 \mathbf{u}$$

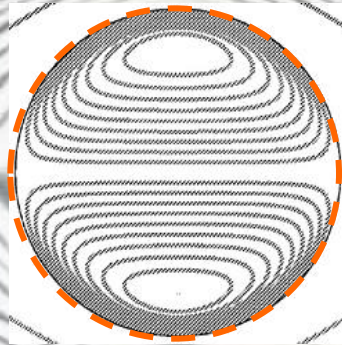
Singular perturbation

$$[[\mathbf{n} \cdot \boldsymbol{\sigma} \cdot \mathbf{n}]] = \gamma \left(\frac{\pi}{4} \kappa + \frac{2}{h} \right)$$

jump in normal stresses

$$[[\mathbf{u} \cdot \mathbf{n}]] = 0$$

continuity of normal velocity



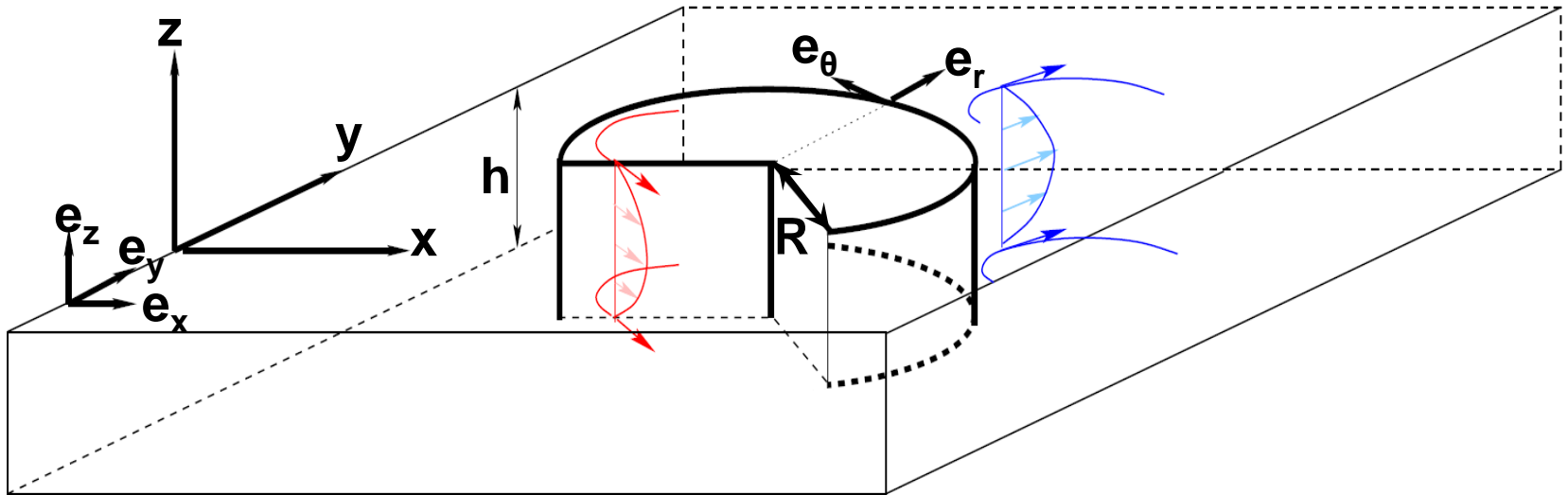
continuity of tangential stress

$$[[\mathbf{t} \cdot \boldsymbol{\sigma} \cdot \mathbf{n}]] = 0$$

continuity of tangential velocity

$$[[\mathbf{u} \cdot \mathbf{t}]] = 0$$

2D Brinkman equations



• Aspect ratio $k = \sqrt{12} R/h \gg 1$

• $w=0$

• Parabolic profiles

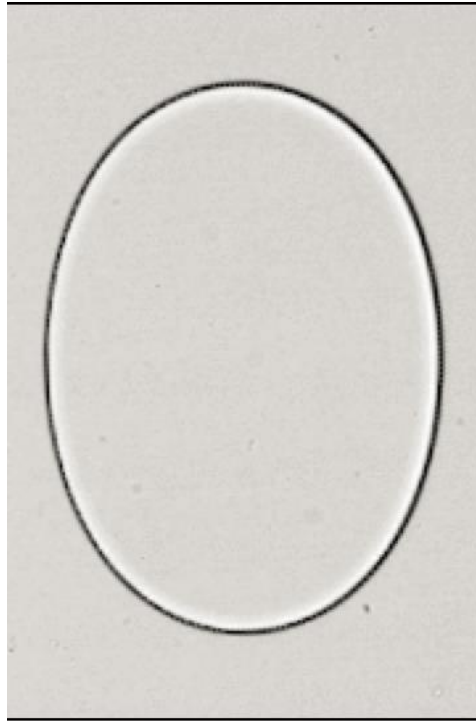
$$\mathbf{v}(x, y, z) = \mathbf{u}(x, y) \frac{6(h - z)}{h^2}$$

Stokes eq.

$$\begin{aligned} \nabla p &= \Delta \mathbf{u} - k^2 \mathbf{u} \\ \text{div} \mathbf{u} &= 0 \end{aligned}$$

Darcy eq.

2D Brinkman equations



$$[[\mathbf{n} \cdot \boldsymbol{\sigma} \cdot \mathbf{n}]] = \gamma \left(\frac{\pi}{4} \kappa + \frac{2}{h} \right)$$

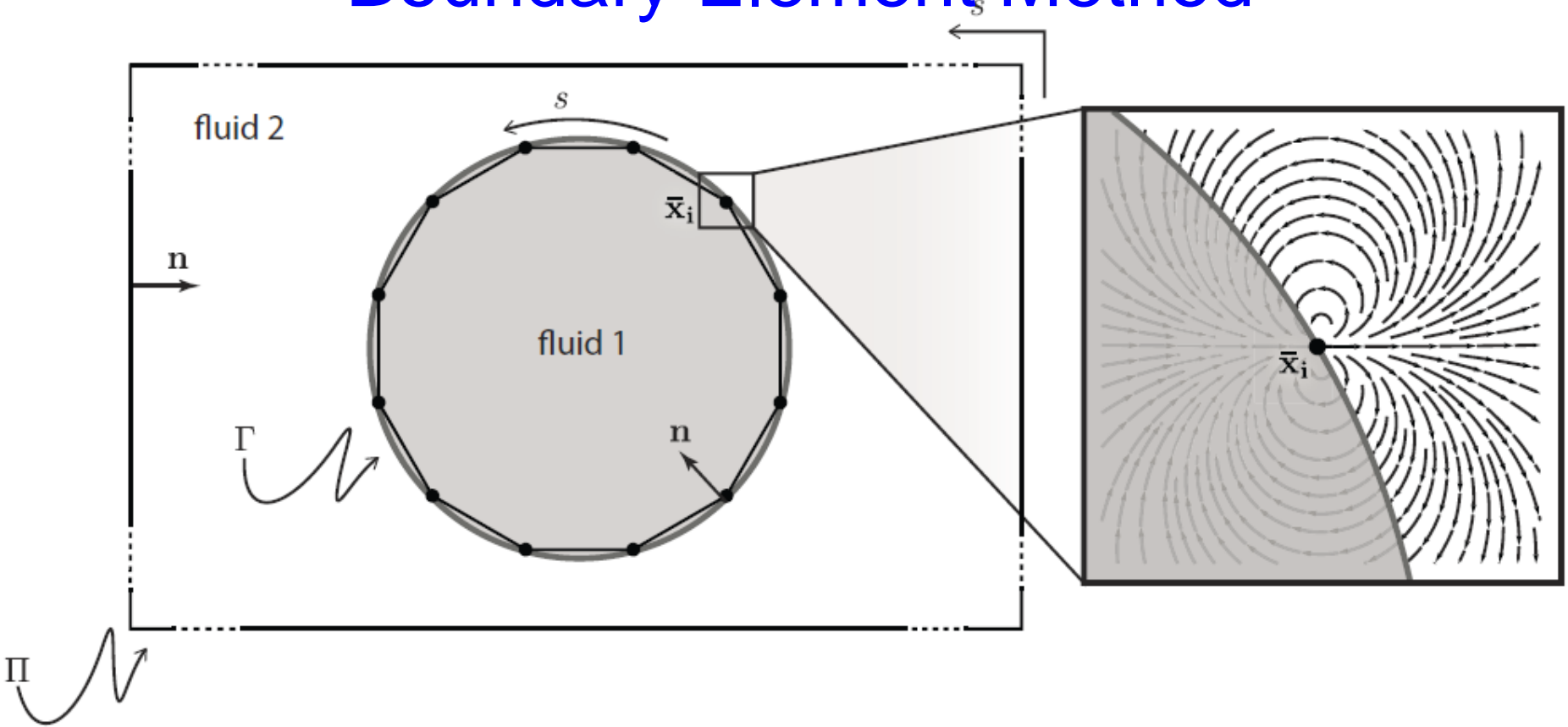
$$[[\mathbf{t} \cdot \boldsymbol{\sigma} \cdot \mathbf{n}]] = 0$$

$$[[\mathbf{u} \cdot \mathbf{n}]] = 0$$

$$[[\mathbf{u} \cdot \mathbf{t}]] = 0$$

$$\begin{aligned} \nabla p &= \Delta \mathbf{u} - k^2 \mathbf{u} \\ \operatorname{div} \mathbf{u} &= 0 \end{aligned}$$

Boundary Element Method



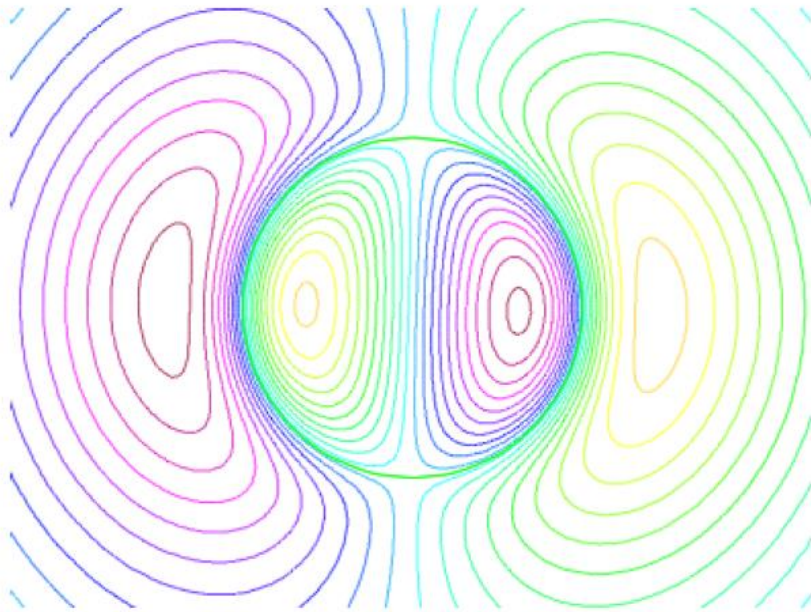
Transformation to boundary integrals

$$\oint_{\Gamma} ([\bar{\sigma} \mathbf{n}] \cdot \mathbf{G} - \mathbf{T} \mathbf{n} \cdot [\mu] \mathbf{u}) ds + \dots = 0$$

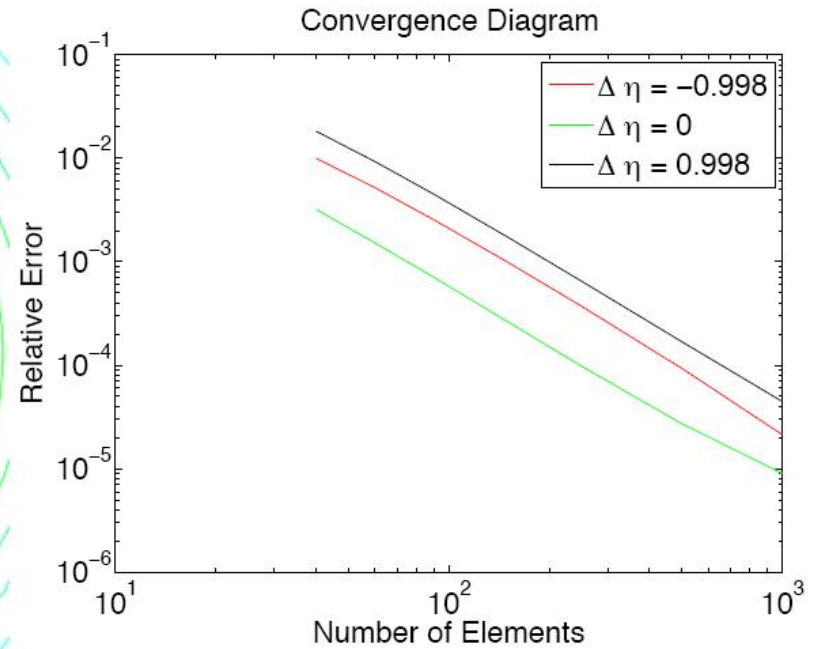
jump in surface stress

difference in viscosity

Validation of boundary element algorithm for Brinkman equations

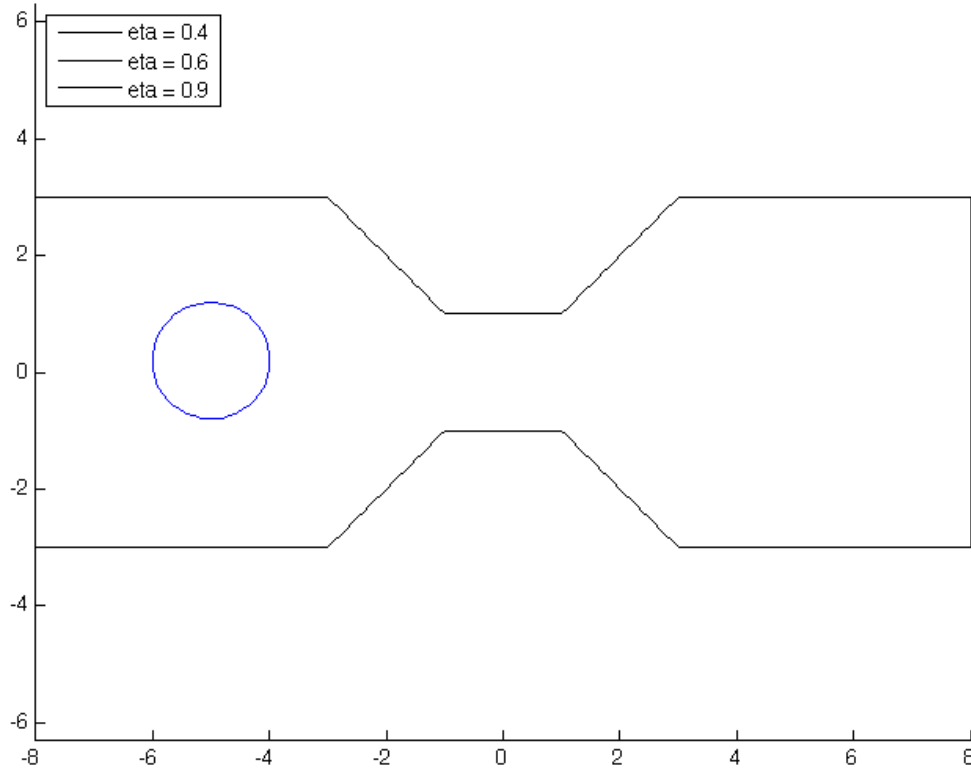


(e) Streamlines: thermo capillary flow



(f) Convergence: thermo capillary flow

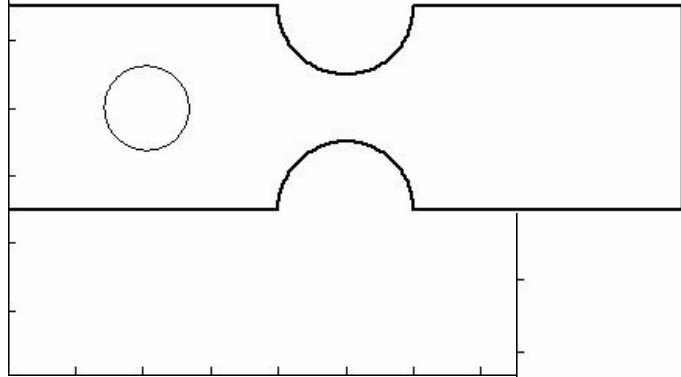
Influence of viscosity ratio



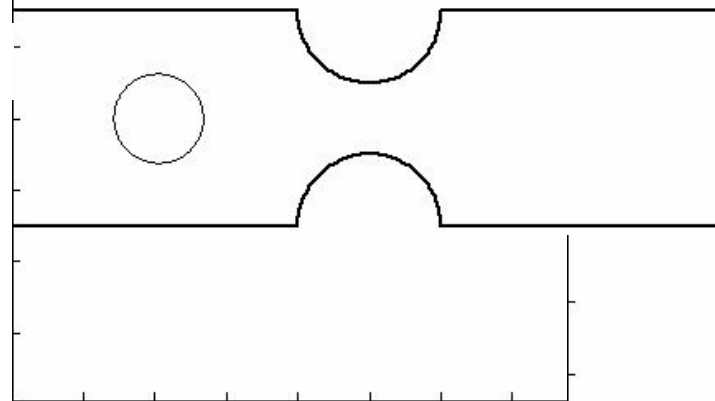
$k=12, Ca=0.1$

Influence of capillary number

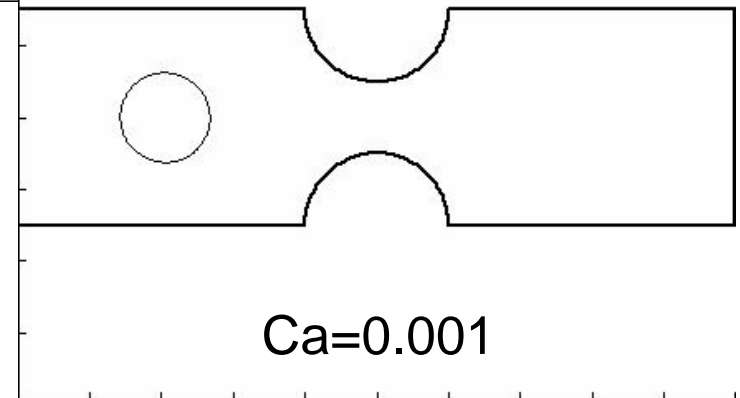
$k=12, \eta=1$



$Ca=0.1$

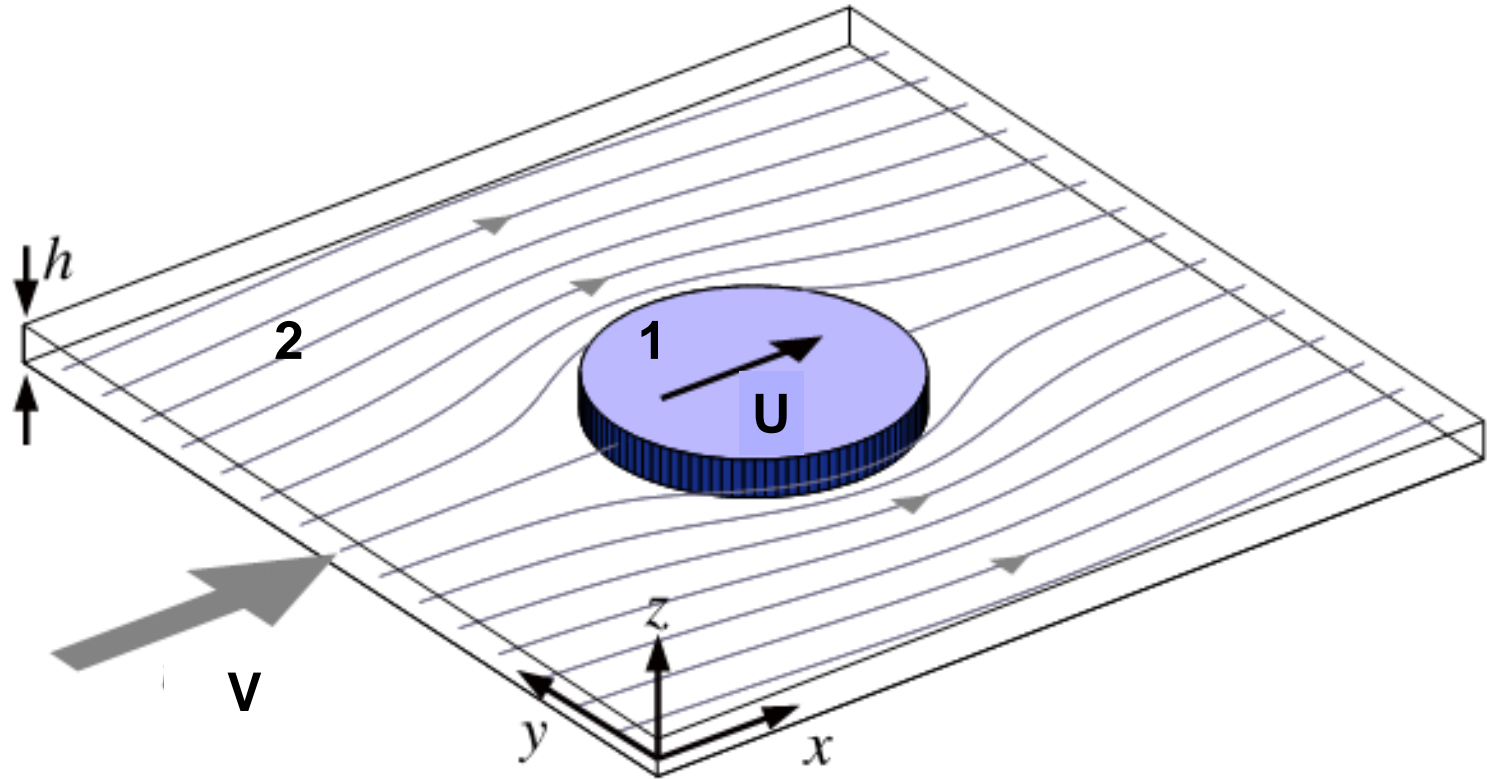


$Ca=0.01$



$Ca=0.001$

Migration velocity for a rigid pancake droplet



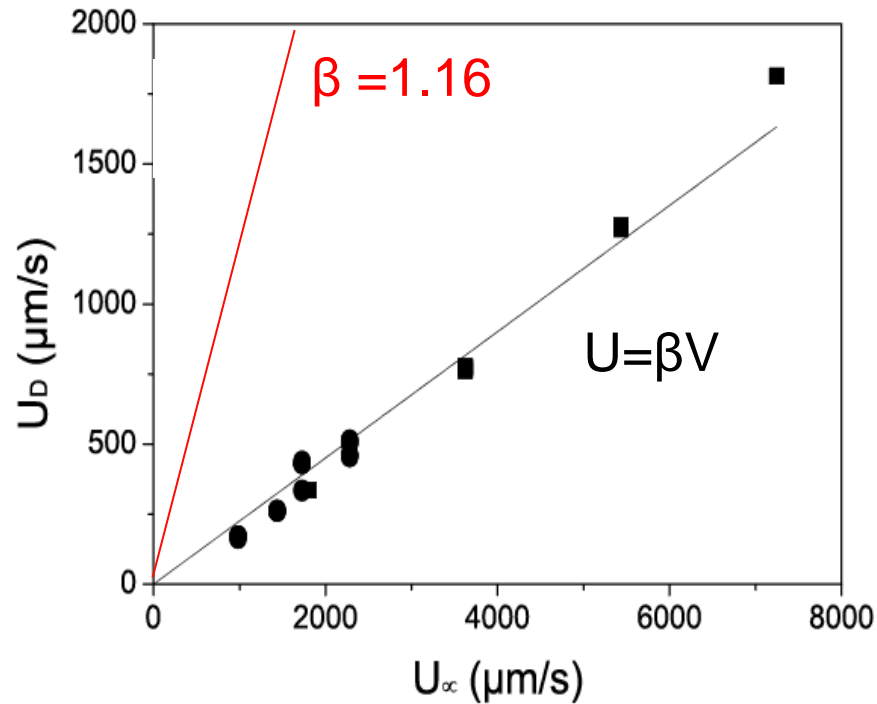
$Ca \ll 1 \Rightarrow$ Freeze the droplet interface

$$U = \frac{2\mu_2}{\mu_1 + \mu_2} V + O(1/k) V$$

mobility β

Brinkman

Recent drop velocity measurements (Leman and Tabeling)

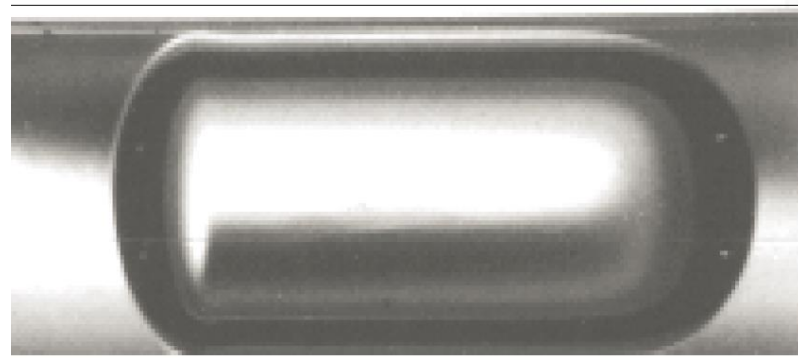
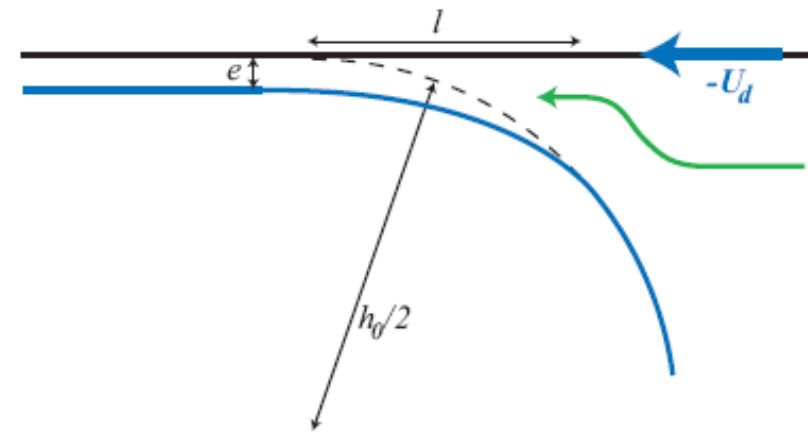
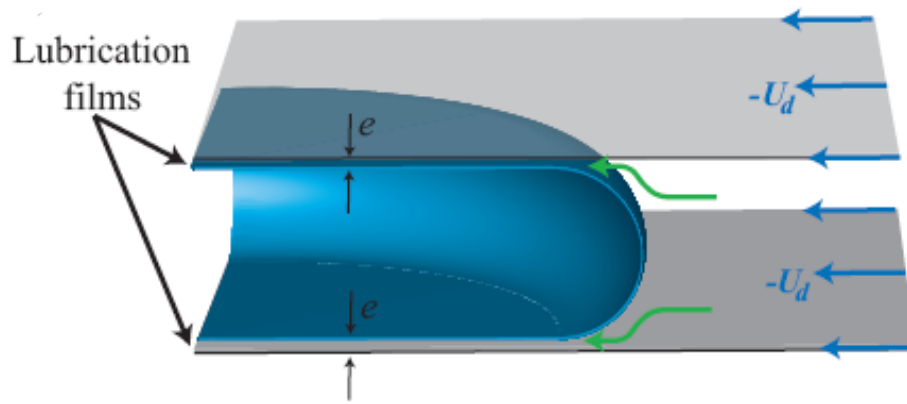


DI water with 1% w/w (SDS) surfactant droplets in fluorinated oil

(■) PDMS system, $h=41\mu\text{m}$, $w_2=500\mu\text{m}$;

(●) NOA system, $h=37\mu\text{m}$, $w_2=3000\mu\text{m}$;

Landau-Levich-Bretherton films

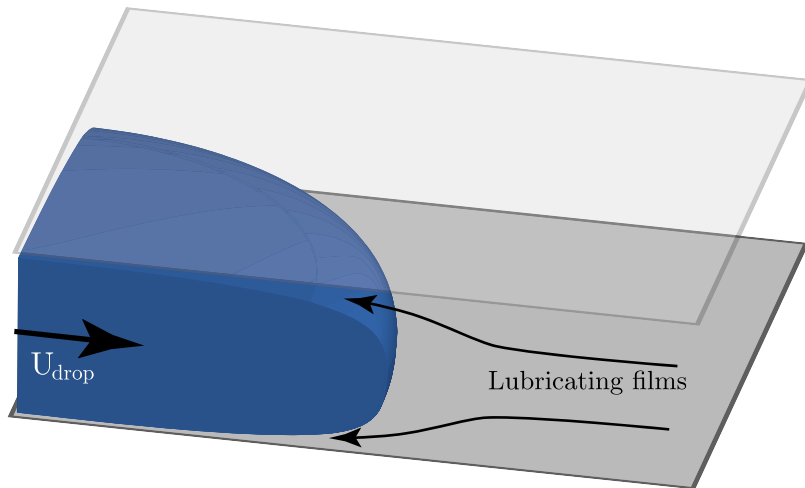


Kreutzer

Asymptotic correction due to dynamic films

$$[[\mathbf{n} \cdot \boldsymbol{\sigma} \cdot \mathbf{n}]] = \gamma \left(\frac{\pi}{4} \kappa + \frac{2}{h} \left(1 + \alpha \text{ca}(\mathbf{x})^{2/3} \right) \right)$$

$$\text{ca}(\mathbf{x}) = \frac{\mu_2 \mathbf{u}(\mathbf{x}) \cdot \mathbf{n}(\mathbf{x})}{\gamma}$$

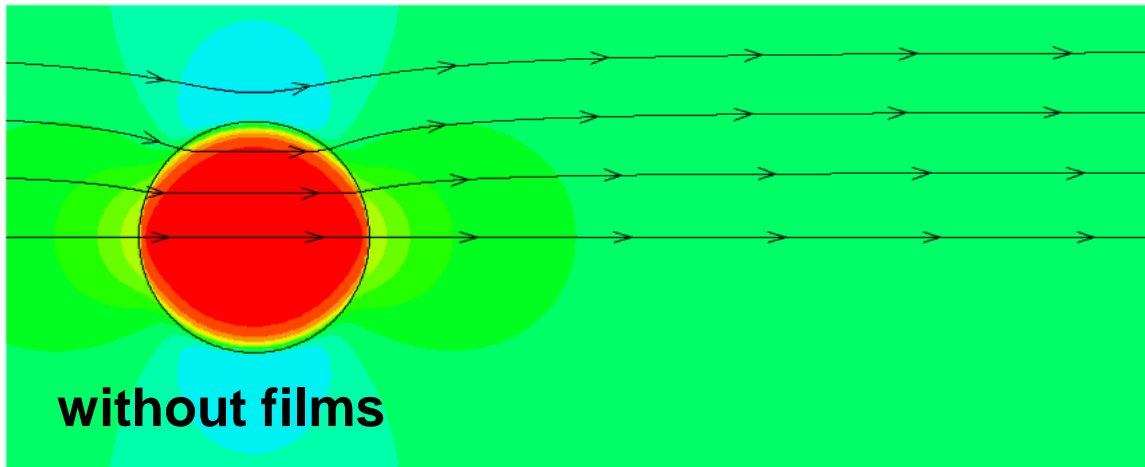


Local capillary number at point \mathbf{x}

Advancing meniscus : $\alpha = 3.8$

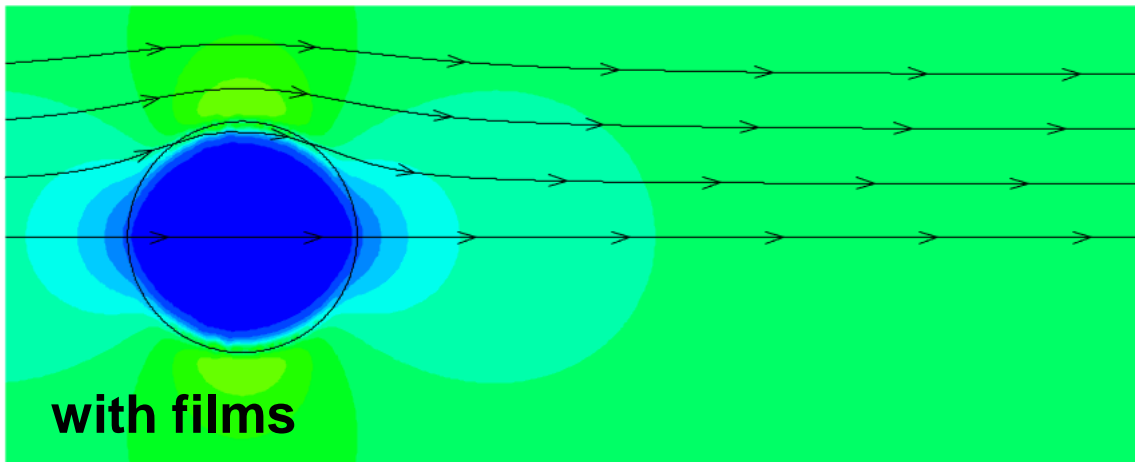
Receding meniscus : $\alpha = -1.13$

Dynamics of deformable droplets



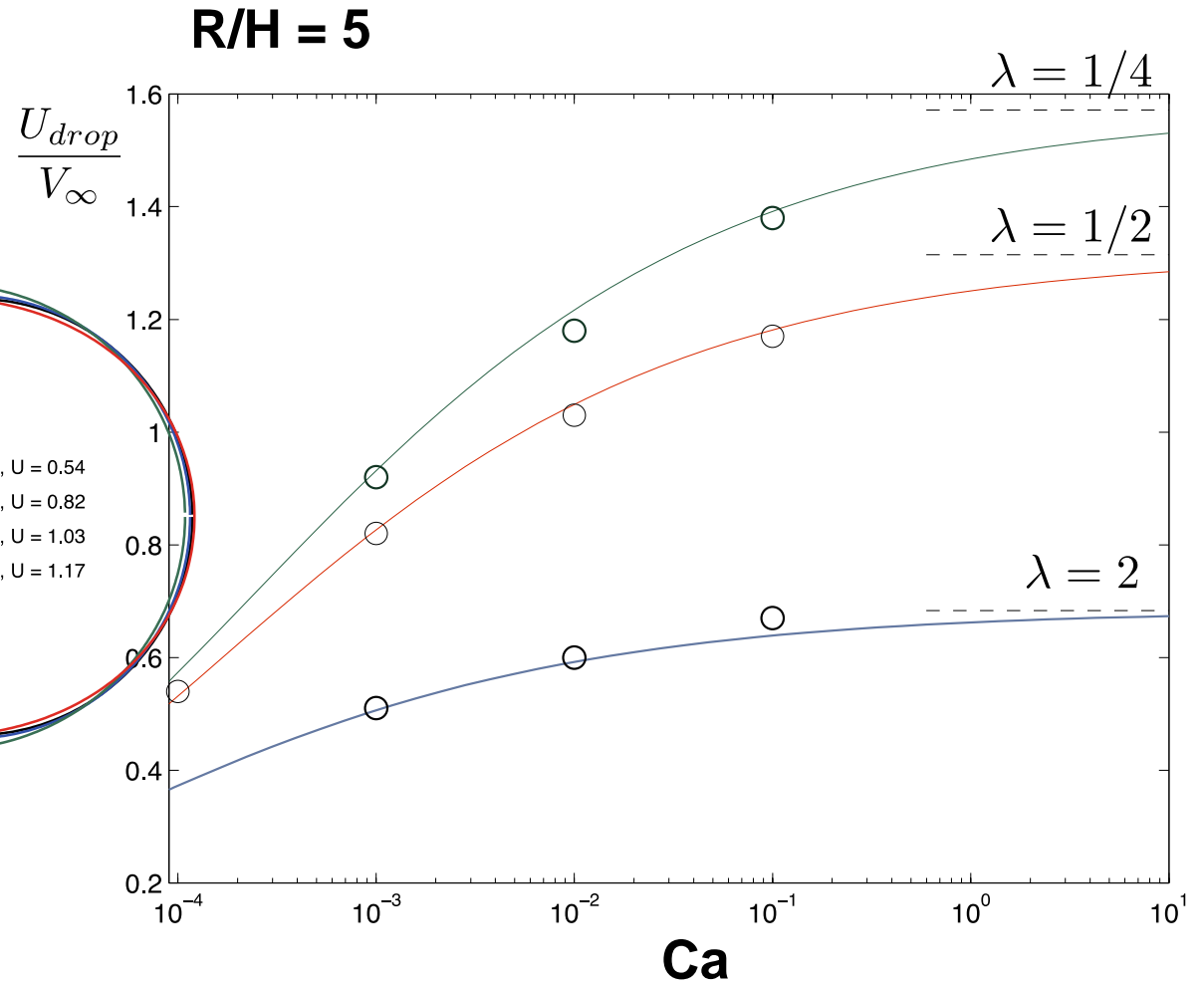
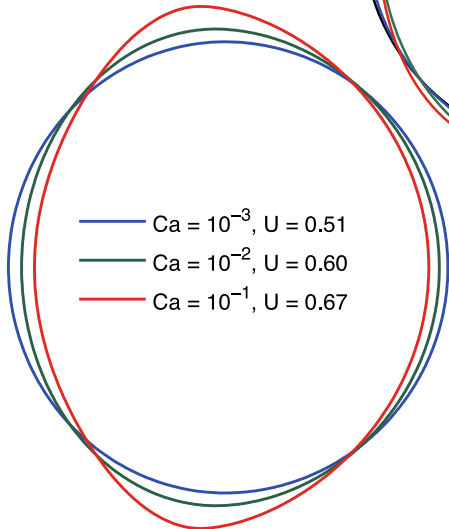
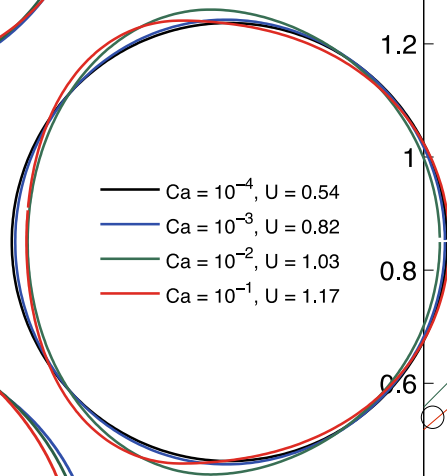
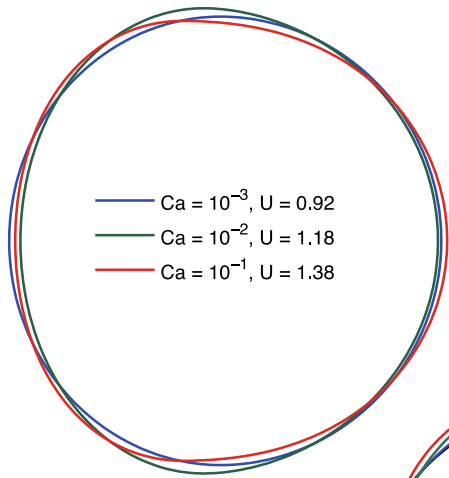
$$U_{drop} = 1.475$$

$$R/H = 5 \quad \lambda = 1/3 \quad Ca = 10^{-4}$$



$$U_{drop} = 0.559$$

Deformable droplets



Assuming that the droplet does not deform

$F_{flow} = 24\pi\mu_2 V \frac{R^2}{h}$

$F_{drop} = 12\pi(\mu_1 + \mu_2) U \frac{R^2}{h}$

$F_{film} = (3.8 + 1.13) \frac{2\Gamma(\frac{1}{3})}{5\sqrt{3}\pi\Gamma(\frac{5}{6})} k\pi \frac{U^{2/3} V^{1/3}}{Ca^{1/3}}$

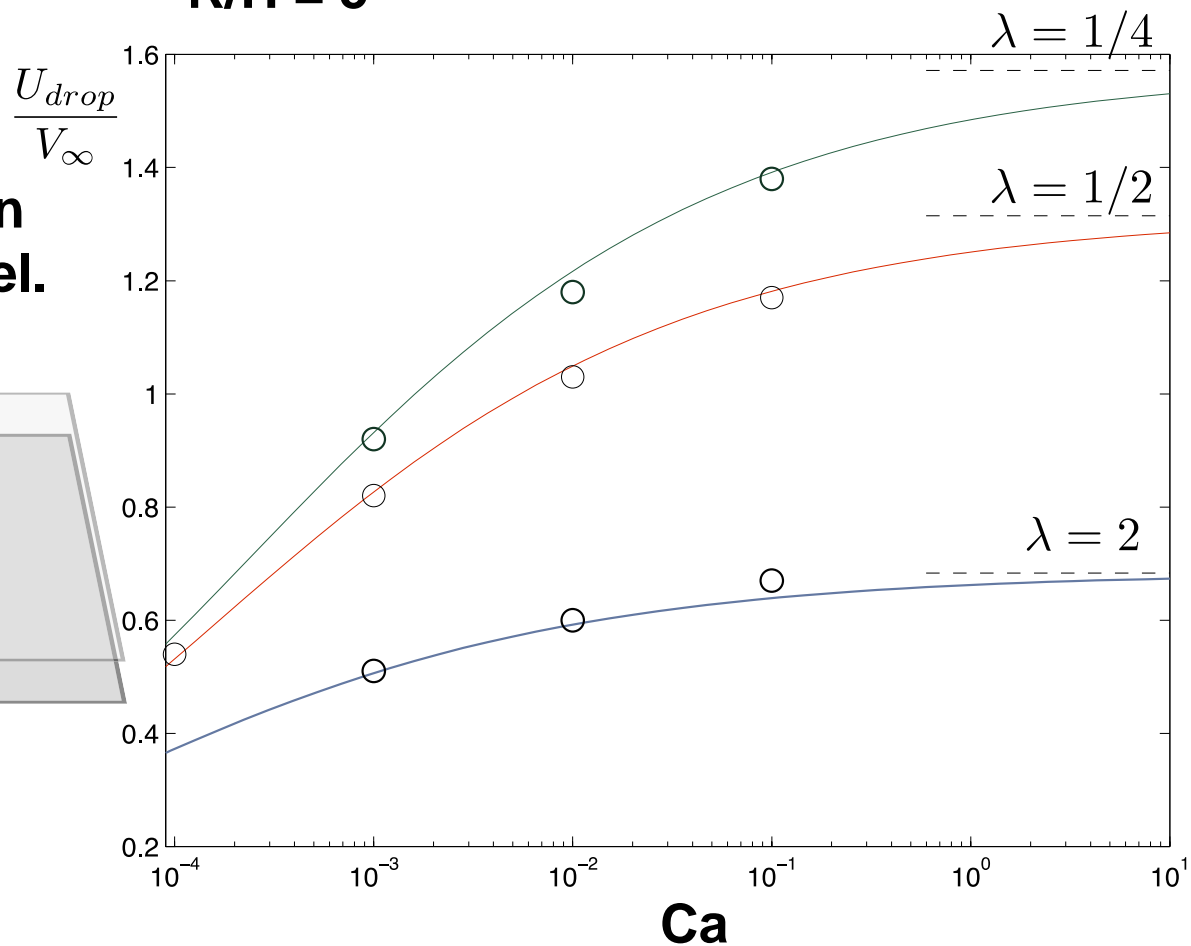
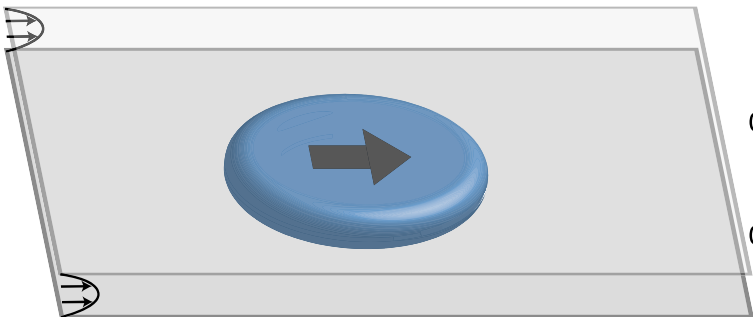
$$\Sigma F = 0$$

$\Rightarrow U$ is a root of a cubic function

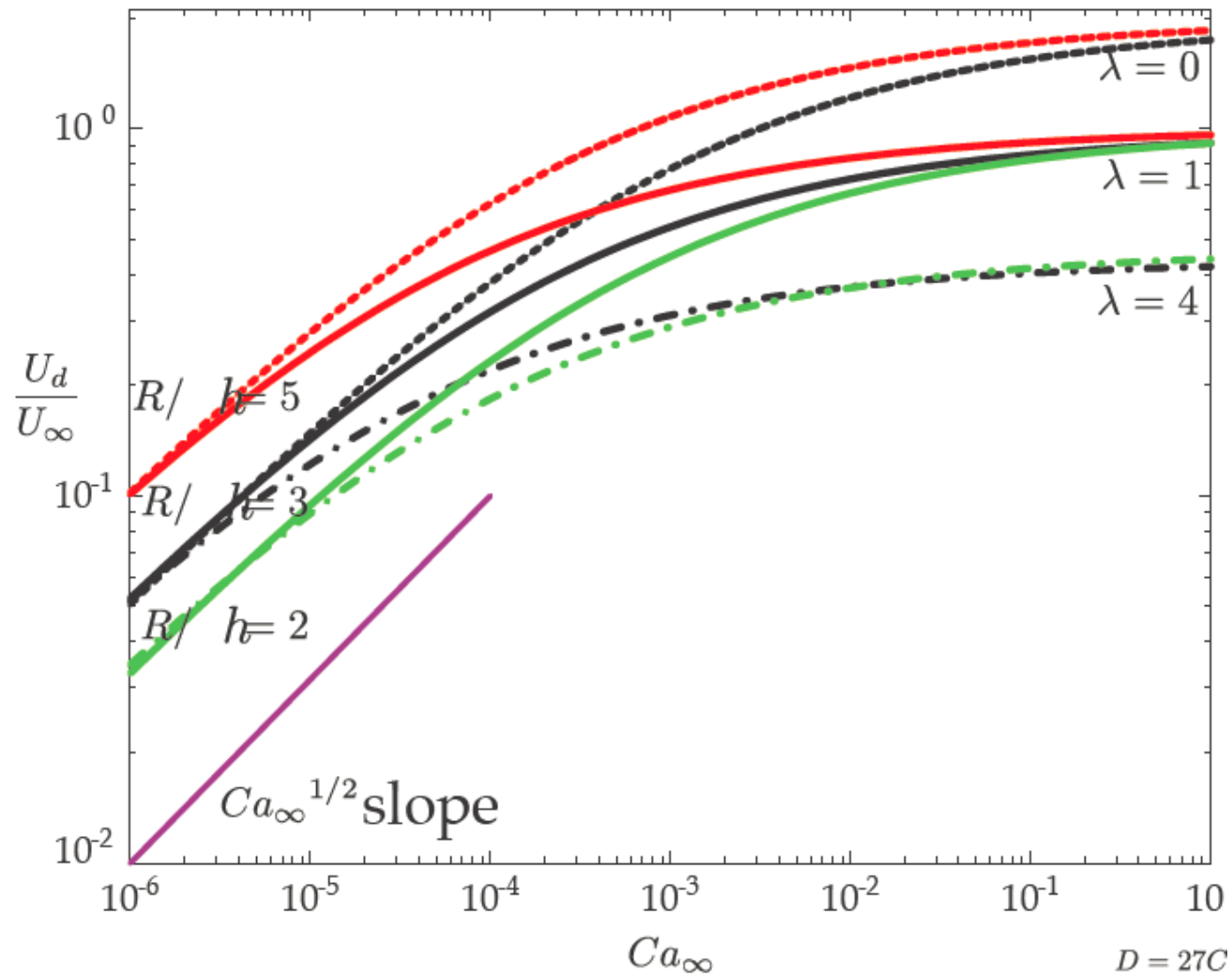
Undeformable droplets

$R/H = 5$

Droplet velocity in an infinitely wide channel.

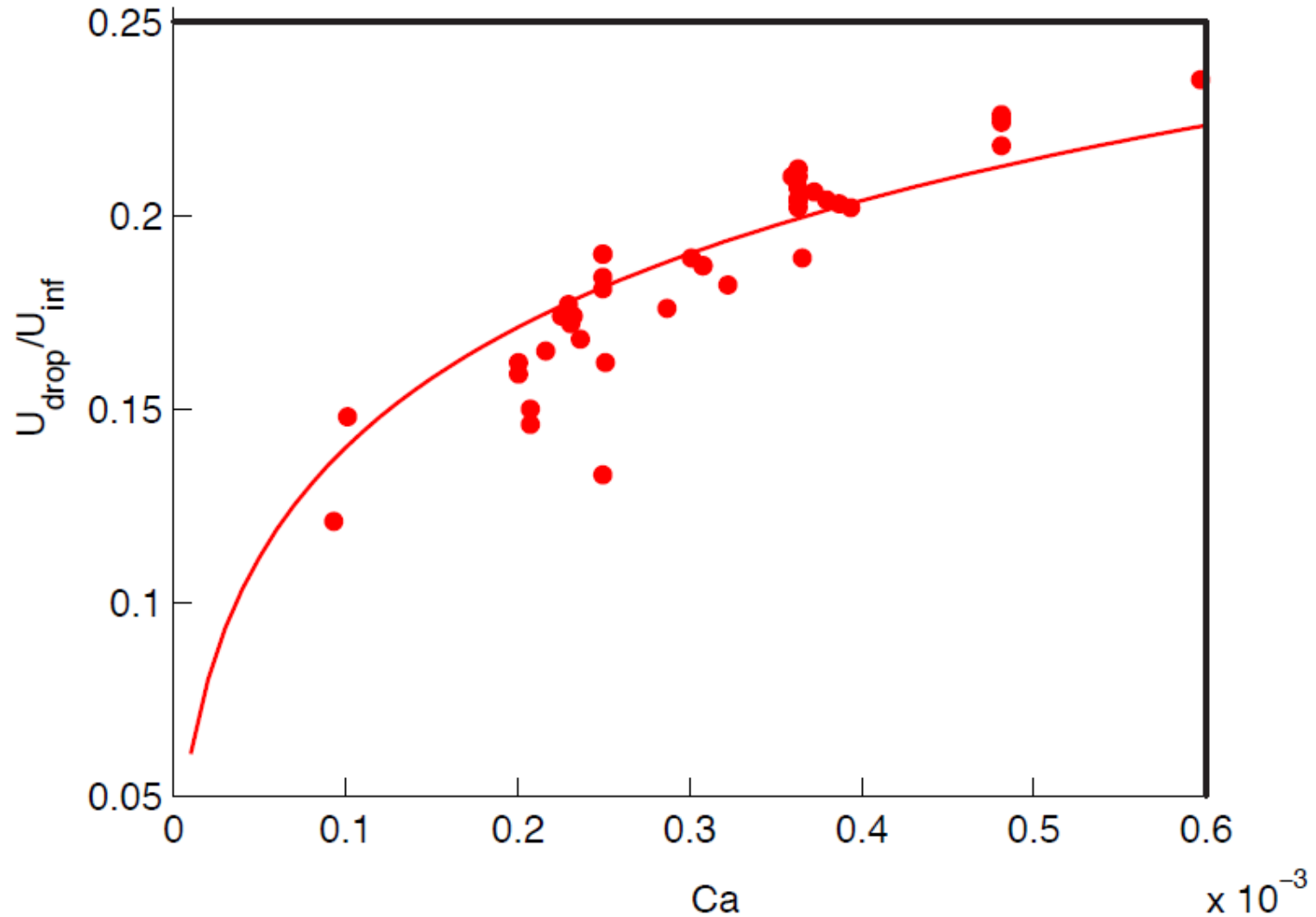


Analytical expression

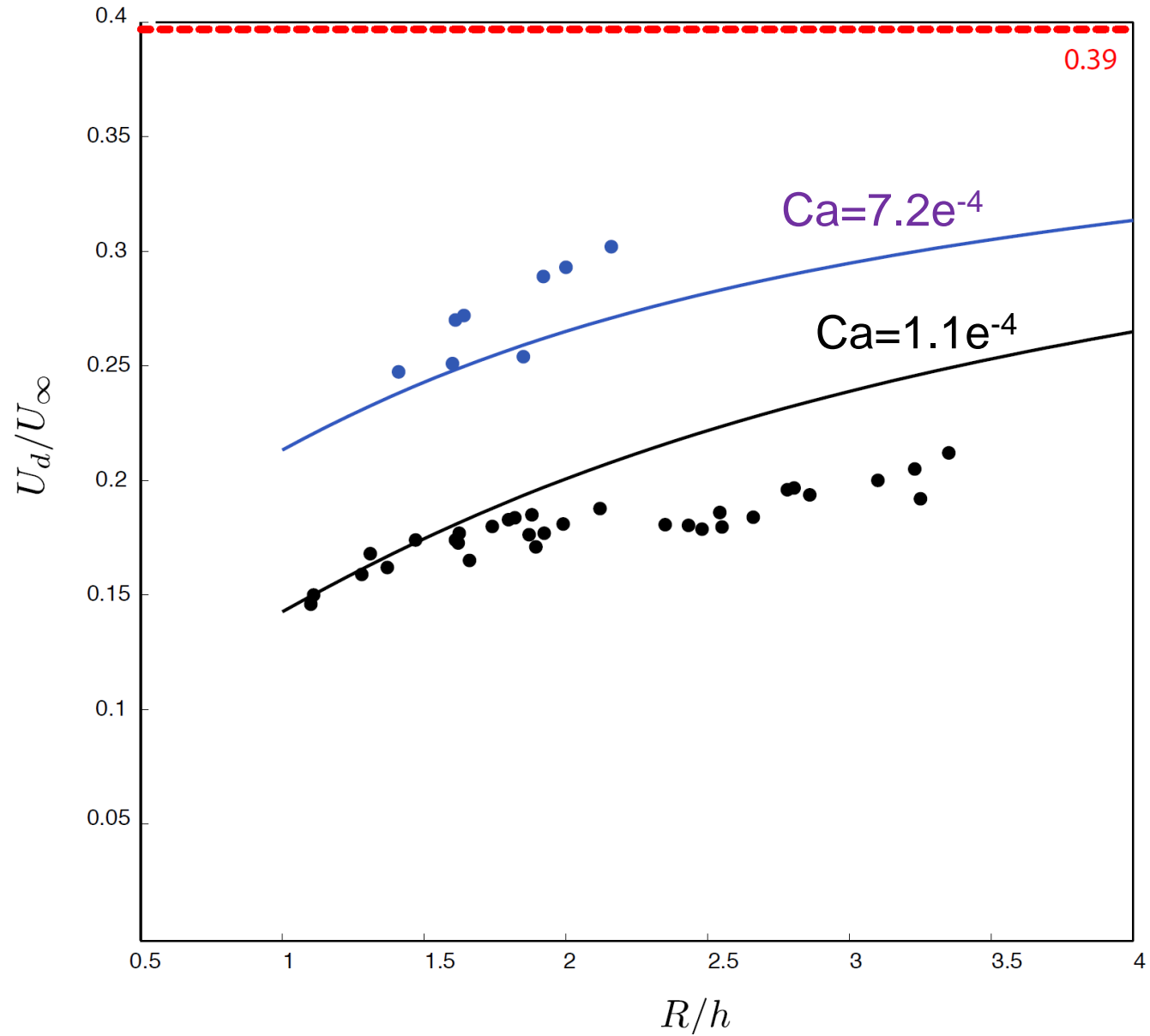


Experimental comparison FC40 droplets in water

$\gamma=53\text{mPa}\cdot\text{m}$, $\mu_1=4.1\text{cSt}$, $R/h = 1.3$



Experimental comparison



Conclusion

In absence of surfactants, the droplet of a velocity can be accurately captured at low Ca